

A6-1
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
BOILER EMISSIONS CRITERIA POLLUTANTS

| | | Maximum Emissions Case (100%) | Pollutant Form | Pollutant Class | |
|---|---|----------------------------------|-------------------|--------------------|---|
| PLANT PERFORMANCE: | | | | | |
| Primary Fuel Feed Rate | Tons/hr | 538 | | | |
| Full load Heat input to Boiler | mmBtu/hr | 8,710 | | | |
| PLANT EMISSION ANALYSIS (for two (2) Boilers at the above specifications): | | | | | Emission Rate² |
| Carbon Monoxide | Short term avg. lb/hr ton/year | 1,742 7,630 | Vapor | Inorganic | 0.1 lb/mmBtu |
| Nitrogen Oxides | 3-hr avg. lb/hr Annual avg. lb/hr tons/year | 1,045 1,045 4,578 | Vapor | Inorganic | 0.06 lb/mmBtu 0.06 lb/mmBtu |
| Particulate Matter (Filterable) ¹ | 24-hour avg. lb/hr tons/year | 174.2 763 | Particulate | Inorganic/Organic | 0.01 lb/mmBtu |
| Particulate Matter (Condensable) ¹ | 24-hour avg. lb/hr tons/year | 174.2 763 | Particulate | Inorganic/Organic | 0.01 lb/mmBtu |
| Total Particulate Matter ¹ | 24-hour avg. lb/hr tons/year | 348.4 1,526 | Particulate | Inorganic/Organic | 0.02 lb/mmBtu |
| Lead | lb/hr tons/year | 0.5 1.976 | Particulate | Inorganic | 2.59E-05 lb/mmBtu |
| Volatile Organic Compounds | Short term avg. lb/hr tons/year | 61.0 267.0 | Vapor | Organic | 0.0035 lb/mmBtu |
| Sulfur Dioxide | 3-hour avg. lb/hr 24-hour avg. lb/hr 30-day avg. lb/hr tons/year | 1,394 1,045 1,045 4,578 | Vapor | Inorganic | 0.08 lb/mmBtu 0.06 lb/mmBtu 0.06 lb/mmBtu |
| Sulfuric Acid Mist | Short term avg. lb/hr ton/year | 69.7 305.2 | Particulate | Organic | 0.004 lb/mmBtu |

STACK PARAMETERS

| | | | |
|--------------------------------|-----------|-----------------|---|
| Stack Flue Gas Temperature | 324 | K | |
| Stack Flue Gas Flow Rate | 3,382,914 | acfm | |
| Stack Flue Gas Flow Rate | 2,246,137 | scfm | |
| Exit Velocity | 55 | ft/s at 100% | (assume velocity is at actual conditions) |
| Height | 727 | ft | |
| Stack diameter (top ID) | 36 | ft | (each boiler stack) |
| Stack top area | 1,022.93 | ft ² | |
| Ash Content | 13 | % | |
| Heat Content | 8100 | Btu/lb | |
| Atmospheric Pressure (Ely, NV) | 23.5867 | in Hg | |

Notes:

1 - Particulate matter less than 10 microns aerodynamic diameter (PM₁₀)

2 - Provided by Cummins & Barnard (March 2007), unless otherwise stated. Matches BACT value.

Atmospheric pressure in Ely, NV is 23.5867 in Hg. Source: "Useful Tables for Engineers and Steam Users" 11th Edition 1969 - Babcock and Wilcox Company.

A6-2
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
DIESEL AUXILIARY BOILER EMISSIONS CRITERIA POLLUTANTS

| Pollutant | Emission Factor | | Source | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Pollutant Form | Pollutant Class |
|---------------------------------------|-----------------|----------|-------------------------|--------------------------|---------------------------|----------------|-----------------------|
| Carbon Monoxide | 0.036 | lb/mmBtu | BACT - confirmed by C&B | 7.92 | 34.69 | Vapor | Inorganic |
| Nitrogen Oxides | 0.1 | lb/mmBtu | BACT | 22.00 | 96.36 | Vapor | Inorganic |
| Particulate Matter (Filterable) | 0.01 | lb/mmBtu | BACT | 2.20 | 9.64 | Particulate | Inorganic/ Organic |
| Particulate Matter (Condensable) | 0.01 | lb/mmBtu | BACT | 2.20 | 9.64 | Particulate | Inorganic/ Organic |
| Total Particulate Matter ¹ | 0.02 | lb/mmBtu | BACT | 4.40 | 19.27 | Particulate | Inorganic/ Organic |
| Volatile Organic Compounds | 0.0018 | lb/mmBtu | BACT | 0.40 | 1.73 | Vapor | Organic |
| Sulfur Dioxide | 0.05 | lb/mmBtu | BACT - confirmed by C&B | 11.00 | 48.18 | Vapor | Inorganic |

| | |
|------------------------|---------|
| Sulfur Content of Fuel | 0.0015% |
|------------------------|---------|

Description: Emission estimate is based on an auxiliary boiler designed to produce 220 mmBtu/hr. The auxiliary boiler will be fired on diesel fuel.

STACK PARAMETERS

| | | | | |
|----------------------------|--------|-----------------|---|---|
| Stack Flue Gas Temperature | 350 | °F | 449.8 | K |
| Stack Flue Gas Flow Rate | 69,208 | acfm | | |
| Stack Flue Gas Flow Rate | 33,129 | scfm | | |
| Exit Velocity | 59.06 | ft/sec | (assume velocity is at actual conditions) | |
| Height | 299.87 | ft | | |
| Stack diameter (top ID) | 4.99 | ft | | |
| Stack area | 19.53 | ft ² | | |

| | | |
|--|----------|------------|
| Maximum Fuel Firing Rate for the Auxiliary Boiler: | 220.0 | mmBtu/hr |
| Heating Value for Diesel Fuel: | 140,000 | Btu/gal |
| Maximum Fuel Firing Rate: | 1,571.43 | gal/hr |
| Estimated Maximum Annual Hours of Operation: | 8,760 | hours/year |
| Atmospheric Pressure (Ely, NV) | 23.5867 | in Hg |

Notes:

¹Particulate matter less than 10 microns aerodynamic (PM₁₀)

Stack height of Auxiliary Boiler is assumed to be 10 ft above height of boiler buildings

Atmospheric pressure in Ely, NV source: "Useful Tables for Engineers and Steam Users" 11th Edition 1969 - Babcock and Wilcox Company.

A6-3
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
PLANT DIESEL ENGINE AUXILIARY GENERATOR EMISSIONS CRITERIA POLLUTANTS

| Pollutant | Emission Factor | Units | Source | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Pollutant Form | Pollutant Class |
|---------------------------------------|-----------------|----------|---|--------------------------|---------------------------|----------------|-------------------|
| Carbon Monoxide | 3.5 | g/kW-hr | 40 CFR Part 89 | 23.1 | 2.89 | Vapor | Inorganic |
| Nitrogen Oxides | 5.6 | g/kW-hr | 40 CFR Part 89, NOx = 87.5% of total NMHC+NOx | 37.0 | 4.6 | Vapor | Inorganic |
| Total Particulate Matter ¹ | 0.2 | g/kW-hr | 40 CFR Part 89 | 1.3 | 0.17 | Particulate | Inorganic/Organic |
| Volatile Organic Compounds | 0.8 | g/kW-hr | 40 CFR Part 89, VOC = 12.5% of total NMHC+NOx | 5.3 | 0.66 | Vapor | Organic |
| Sulfur Dioxide | 0.0016 | lb/mmBtu | C&B | 0.019 | 0.0024 | Vapor | Inorganic |

| | |
|------------------------|---------|
| Sulfur Content of Fuel | 0.0015% |
|------------------------|---------|

Description: Emission estimates based on a 3 MW emergency diesel generator using No. 2 fuel oil. Calculations are based on 40 CFR Part 89, Tier 2 limits KW>560, except SO₂ which was calculated by Cummins & Barnard for low sulfur fuel.

STACK PARAMETERS

| | | | |
|------------------------------------|---------|-----------------|-----------------|
| Stack Flue Gas Temperature | 711 | K | |
| Flow Rate | 56,871 | acfm | |
| Flow Rate | 17,225 | scfm | |
| Exit Velocity | 72.2 | ft/sec | |
| Height | 20.0 | ft | |
| Stack diameter (top ID) | 27 | inch | |
| Stack area | 3.98 | ft ² | |
| Diesel engine output: | 3000 | kw | |
| Diesel engine output: | 4650 | hp | 1hp=2546 Btu/hr |
| Diesel engine output: | 11.84 | mmBtu/hr | |
| Diesel engine input: | 138.9 | gal/hr | |
| Diesel engine input: | 19.0 | mmBtu/hr | |
| Maximum Annual Hours of Operation: | 250 | hours/year | |
| Atmospheric Pressure (Ely, NV) | 23.5867 | in Hg | |

Notes:

¹Particulate matter less than 10 microns aerodynamic (PM₁₀)

Stack temperatures, velocities and fuel usage rates obtained from Caterpillar data sheets.

Stack heights and diameters are based on engineering estimates.

Average heating value of diesel fuel oil is assumed to be 19,300 Btu/lb with a density of 7.1 lb/gal. Based on AP-42 Table 3.4-1.

Atmospheric pressure in Ely, NV source: "Useful Tables for Engineers and Steam Users" 11th Edition 1969 - Babcock and Wilcox Company.

A6-4
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
DIESEL FIRE WATER PUMP EMISSIONS CRITERIA POLLUTANTS

| Pollutant | Emission Factor | Units | Source | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Pollutant Form | Pollutant Class |
|---------------------------------------|-----------------|----------|---|--------------------------|---------------------------|----------------|-------------------|
| Carbon Monoxide | 2.6 | g/hp-hr | Subpart IIII Table 4 | 4.5 | 0.564 | Vapor | Inorganic |
| Nitrogen Oxides | 4.2 | g/hp-hr | Subpart IIII Table 4, NO _x = 87.5% of total NMHC+NO _x | 7.3 | 0.911 | Vapor | Inorganic |
| Total Particulate Matter ¹ | 0.15 | g/hp-hr | Subpart IIII Table 4 | 0.3 | 0.0326 | Particulate | Inorganic/Organic |
| Volatile Organic Compounds | 0.6 | g/hp-hr | Subpart IIII Table 4, VOC = 12.5% of total NMHC+NO _x | 1.0 | 0.130 | Vapor | Organic |
| Sulfur Dioxide | 0.0016 | lb/mmBtu | C&B | 0.003 | 0.0004 | Vapor | Inorganic |

| | |
|------------------------|---------|
| Sulfur Content of Fuel | 0.0015% |
|------------------------|---------|

Description: Emission estimates based on a 787.5 hp emergency diesel fire pump using No. 2 fuel oil. Calculations are based on Federal Register, Vol. 71, No. 132, 40 CFR Subpart IIII, 2009+ KW>560, except SO₂ which was calculated by Cummins & Barnard for low sulfur fuel.

STACK PARAMETERS

| | | | |
|------------------------------------|---------|-----------------|-----------------|
| Stack Flue Gas Temperature | 836 | K | |
| Flow Rate | 15,970 | acfm | |
| Flow Rate | 4,111 | scfm | |
| Exit Velocity | 87.2 | ft/sec | |
| Height | 10.0 | ft | |
| Stack diameter (top ID) | 12 | inch | |
| Stack area | 0.79 | ft ² | |
| Diesel engine output: | 788 | hp | 1hp=2546 Btu/hr |
| Diesel engine output: | 2.01 | mmBtu/hr | |
| Diesel engine input: | 33 | gal/hr | |
| Diesel engine input: | 4.5 | mmBtu/hr | |
| Maximum Annual Hours of Operation: | 250 | hours/year | |
| Atmospheric Pressure (Ely, NV) | 23.5867 | in Hg | |

Notes:

¹ Total particulate matter less than 10 microns aerodynamic (PM₁₀). No distribution of filterable versus condensable PM₁₀ was available.

Stack temperatures, velocities and fuel usage rates obtained from Caterpillar data sheets.

Stack heights and diameters are based on engineering estimates.

Average heating value of diesel fuel oil is assumed to be 19,300 Btu/lb with a density of 7.1 lb/gal.

Atmospheric pressure in Ely, NV source: "Useful Tables for Engineers and Steam Users" 11th Edition 1969 - Babcock and Wilcox Company.

A6-5
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
DIESEL BOOSTER FIRE PUMP EMISSIONS CRITERIA POLLUTANTS

| Pollutant | Emission Factor | Units | Source | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Pollutant Form | Pollutant Class |
|---------------------------------------|-----------------|----------|---|--------------------------|---------------------------|----------------|-------------------|
| Carbon Monoxide | 3.7 | g/hp-hr | Subpart IIII Table 4 | 0.7 | 0.0918 | Vapor | Inorganic |
| Nitrogen Oxides | 3.1325 | g/hp-hr | Subpart IIII Table 4, NO _x = 87.5% of total NMHC+NO _x | 0.6 | 0.0777 | Vapor | Inorganic |
| Total Particulate Matter ¹ | 0.3 | g/hp-hr | Subpart IIII Table 4 | 0.1 | 0.0074 | Particulate | Inorganic/Organic |
| Volatile Organic Compounds | 0.4375 | g/hp-hr | Subpart IIII Table 4, VOC = 12.5% of total NMHC+NO _x | 0.1 | 0.0109 | Vapor | Organic |
| Sulfur Dioxide | 0.0016 | lb/mmBtu | C&B | 0.0004 | 0.00005 | Vapor | Inorganic |

| | |
|------------------------|---------|
| Sulfur Content of Fuel | 0.0015% |
|------------------------|---------|

Description: Emission estimates based on a 90 hp emergency diesel fire pump using No. 2 fuel oil. Calculations are based on Federal Register, Vol. 71, No. 132, 40 CFR Subpart IIII, 20119+ 56=KW=75, except SO₂ which was calculated by Cummins & Barnard for low sulfur fuel.

STACK PARAMETERS

| | | | |
|------------------------------------|---------|-----------------|-----------------|
| Stack Flue Gas Temperature | 308 | K | |
| Flow Rate | 518 | acfm | |
| Flow Rate | 362 | scfm | |
| Exit Velocity | 17.3 | ft/sec | |
| Height | 10.0 | ft | |
| Stack diameter (top ID) | 8 | inch | |
| Stack area | 0.35 | ft ² | |
| Diesel engine output: | 90 | hp | 1hp=2546 Btu/hr |
| Diesel engine output: | 0.23 | mmBtu/hr | |
| Diesel engine input: | 4.2 | gal/hr | |
| Diesel engine input: | 0.6 | mmBtu/hr | |
| Maximum Annual Hours of Operation: | 250 | hours/year | |
| Atmospheric Pressure (Ely, NV) | 23.5867 | in Hg | |

Notes:

¹ Total particulate matter less than 10 microns aerodynamic (PM₁₀). No distribution of filterable versus condensable PM₁₀ was available.
Stack temperatures, velocities and fuel usage rates obtained from Caterpillar data sheets.
Stack heights and diameters are based on engineering estimates.
Average heating value of diesel fuel oil is assumed to be 19,300 Btu/lb with a density of 7.1 lb/gal.
Atmospheric pressure in Ely, NV source: "Useful Tables for Engineers and Steam Users" 11th Edition 1969 - Babcock and Wilcox Company.

A6-6
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
LOCOMOTIVE EMISSIONS CRITERIA POLLUTANTS

| Pollutant | Emission Factor | Units | Source | Per Engine ¹ | | Per 3 Engines ¹ | | Per 6 Engines ¹ | | Pollutant Form | Pollutant Class |
|---------------------------------------|-----------------|----------|--|--------------------------|---------------------------|----------------------------|---------------------------|----------------------------|---------------------------|----------------|-----------------------|
| | | | | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | | |
| Carbon Monoxide | 2.20 | g/bhp-hr | USEPA Tier 1 Emission Standards ² | 1.94 | 8.50 | 5.8 | 25.5 | 11.6 | 51.0 | Vapor | Inorganic |
| Nitrogen Oxides | 7.40 | g/bhp-hr | USEPA Tier 1 Emission Standards ² | 6.53 | 28.58 | 19.6 | 85.7 | 39.2 | 171.5 | Vapor | Inorganic |
| Total Particulate Matter ³ | 0.45 | g/bhp-hr | USEPA Tier 1 Emission Standards ² | 0.40 | 1.74 | 1.2 | 5.2 | 2.4 | 10.4 | Particulate | Inorganic/ Organic |
| Volatile Organic Compounds | 0.55 | g/bhp-hr | USEPA Tier 1 Emission Standards ² | 0.49 | 2.12 | 1.5 | 6.4 | 2.9 | 12.7 | Vapor | Organic |
| Sulfur Dioxide | 0.075 | lb/hr | C&B | 0.08 | 0.33 | 0.2 | 1.0 | 0.45 | 2.0 | Vapor | Organic |

| | |
|------------------------|---------|
| Sulfur Content of Fuel | 0.0015% |
|------------------------|---------|

STACK PARAMETERS

| | | | | |
|----------------------------|--------|-----------------|---|---|
| Stack Flue Gas Temperature | 800 | °F | 700.0 | K |
| Stack Flue Gas Flow Rate | 28,611 | acfm | | |
| Stack Flue Gas Flow Rate | 8,801 | scfm | (assume velocity is at standard conditions) | |
| Exit Velocity | 83 | ft/sec | | |
| Height | 20.0 | ft | | |
| Stack diameter (top ID) | 18 | inch | | |
| Stack area | 1.77 | ft ² | | |

| | | | |
|------------------------------------|---------|------------|-----------------|
| Engine Size | 4000 | hp | C&B |
| Engine Efficiency | 10 | % | Idle C&B |
| Line-Haul Idle horsepower rating | 400 | HP | |
| Diesel engine output: | 1.02 | mmBtu/hr | 1hp=2546 Btu/hr |
| Diesel engine input: | 34.8 | gal/hr | |
| Diesel engine input: | 4.8 | mmBtu/hr | |
| Maximum Annual Hours of Operation: | 8760 | hours/year | |
| Atmospheric Pressure (Ely, NV) | 23.5867 | in Hg | |

A6-7
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
SWITCHYARD DIESEL ENGINE AUXILIARY GENERATOR EMISSIONS CRITERIA POLLUTANTS

| Pollutant | Emission Factor | Units | Source | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Pollutant Form | Pollutant Class |
|---------------------------------------|-----------------|----------|---|--------------------------|---------------------------|----------------|-------------------|
| Carbon Monoxide | 3.5 | g/kW-hr | 40 CFR Part 89 | 5.8 | 0.72 | Vapor | Inorganic |
| Nitrogen Oxides | 5.6 | g/kW-hr | 40 CFR Part 89, NO _x = 87.5% of total NMHC+NO _x | 9.3 | 1.2 | Vapor | Inorganic |
| Total Particulate Matter ¹ | 0.2 | g/kW-hr | 40 CFR Part 89 | 0.3 | 0.041 | Particulate | Inorganic/Organic |
| Volatile Organic Compounds | 0.8 | g/kW-hr | 40 CFR Part 89, VOC = 12.5% of total NMHC+NO _x | 1.3 | 0.165 | Vapor | Organic |
| Sulfur Dioxide | 0.0016 | lb/MMbtu | 40 CFR Part 89 | 0.004 | 0.0005 | Vapor | Inorganic |

| | |
|------------------------|---------|
| Sulfur Content of Fuel | 0.0015% |
|------------------------|---------|

Description: Emission estimates based on a 750 kW emergency diesel generator using No. 2 fuel oil. Calculations are based on 40 CFR Part 89, Tier 2 limits KW>560, except SO₂ which was calculated by Cummins & Barnard for low sulfur fuel.

STACK PARAMETERS

| | | | |
|------------------------------------|---------|-----------------|-----------------|
| Stack Flue Gas Temperature | 805 | K | |
| Flow Rate | 17,901 | acfm | |
| Flow Rate | 4,786 | scfm | |
| Exit Velocity | 74.6 | ft/sec | |
| Height | 20.0 | ft | |
| Stack diameter (top ID) | 14 | inch | |
| Stack area | 1.07 | ft ² | |
| Diesel engine output: | 750 | kW | |
| Diesel engine output: | 1013 | hp | 1hp=2546 Btu/hr |
| Diesel engine output: | 2.58 | mmBtu/hr | |
| Diesel engine input: | 37.4 | gal/hr | |
| Diesel engine input: | 5.1 | mmBtu/hr | |
| Maximum Annual Hours of Operation: | 250 | hours/year | |
| Atmospheric Pressure (Ely, NV) | 23.5867 | in Hg | |

Notes:

¹Particulate matter less than 10 microns aerodynamic (PM₁₀)
Stack temperatures, velocities and fuel usage rates obtained from Caterpillar data sheets.
Stack heights and diameters are based on engineering estimates.
Average heating value of diesel fuel oil is assumed to be 19,300 Btu/lb with a density of 7.1 lb/gal.

A6-8
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
DIESEL SO2 ABSORBER EMERGENCY QUENCH PUMP EMISSIONS CRITERIA POLLUTANTS

| Pollutant | Emission Factor | Units | Source | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Pollutant Form | Pollutant Class |
|---------------------------------------|-----------------|----------|---|--------------------------|---------------------------|----------------|-------------------|
| Carbon Monoxide | 2.6 | g/hp-hr | Subpart IIII Table 4 | 3.9 | 0.49 | Vapor | Inorganic |
| Nitrogen Oxides | 2.625 | g/hp-hr | Subpart IIII Table 4, NO _x = 87.5% of total NMHC+NO _x | 3.9 | 0.5 | Vapor | Inorganic |
| Total Particulate Matter ¹ | 0.15 | g/hp-hr | Subpart IIII Table 4 | 0.2 | 0.03 | Particulate | Inorganic/Organic |
| Volatile Organic Compounds | 0.375 | g/hp-hr | Subpart IIII Table 4, VOC = 12.5% of total NMHC+NO _x | 0.6 | 0.07 | Vapor | Organic |
| Sulfur Dioxide | 0.0016 | lb/mmBtu | C&B | 0.003 | 0.0003 | Vapor | Inorganic |

| | |
|------------------------|---------|
| Sulfur Content of Fuel | 0.0015% |
|------------------------|---------|

Description: Emission estimates based on a 682.5 hp emergency diesel fire pump using No. 2 fuel oil. Calculations are based on Federal Register, Vol. 71, No. 132, 40 CFR Subpart IIII, 2009+ 450=KW=560, except SO₂ which was calculated by Cummins & Barnard for low sulfur fuel.

STACK PARAMETERS

| | | | | |
|------------------------------------|---------|-----------------|-----------------|--|
| Stack Flue Gas Temperature | 811 | K | | |
| Flow Rate | 11,675 | acfm | | |
| Flow Rate | 3,100 | scfm | | |
| Exit Velocity | 65.8 | ft/sec | | |
| Height | 10.0 | ft | | |
| Stack diameter (top ID) | 12 | inch | | |
| Stack area | 0.79 | ft ² | | |
| Diesel engine output: | 683 | hp | 1hp=2546 Btu/hr | |
| Diesel engine output: | 1.74 | mmBtu/hr | | |
| Diesel engine input: | 29.1 | gal/hr | | |
| Diesel engine input: | 4.0 | mmBtu/hr | | |
| Maximum Annual Hours of Operation: | 250 | hours/year | | |
| Atmospheric Pressure (Ely, NV) | 23.5867 | in Hg | | |

Notes:

¹Particulate matter less than 10 microns aerodynamic (PM₁₀)

Stack temperatures, velocities and fuel usage rates obtained from Caterpillar data sheets.

Stack heights and diameters are based on engineering estimates.

Average heating value of diesel fuel oil is assumed to be 19,300 Btu/lb with a density of 7.1 lb/gal.

Atmospheric pressure in Ely, NV source: "Useful Tables for Engineers and Steam Users" 11th Edition 1969 - Babcock and Wilcox Company.

A6-9
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
PROPANE SPARK AUXILIARY GENERATOR EMISSIONS CRITERIA POLLUTANTS

| Pollutant | Emission Factor ² | Units | Source | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Pollutant Form | Pollutant Class |
|--|------------------------------|-------|--------|--------------------------|---------------------------|----------------|-------------------|
| Carbon Monoxide | 0.032 | lb/hr | C&B | 0.032 | 0.06 | Vapor | Inorganic |
| Nitrogen Oxides | 0.19 | lb/hr | C&B | 0.19 | 0.38 | Vapor | Inorganic |
| Filterable Particulate Matter ¹ | 0.006 | lb/hr | C&B | 0.006 | 0.01 | Particulate | Inorganic/Organic |
| Volatile Organic Compounds | 0.005 | lb/hr | C&B | 0.005 | 0.01 | Vapor | Organic |
| Sulfur Dioxide | 0.015 | lb/hr | C&B | 0.015 | 0.03 | Vapor | Inorganic |

| | | | |
|------------------------|------|------------------------|-----|
| Sulfur Content of Fuel | 15.0 | gr/100 ft ³ | C&B |
|------------------------|------|------------------------|-----|

Description:

Emission factors for propane were provided by C&B.

STACK PARAMETERS (C&B)

| | | |
|----------------------------|-------|-----------------|
| Stack Flue Gas Temperature | 901 | K |
| Flow rate | 2,069 | acfm |
| Flow rate | 494 | scfm |
| Exit Velocity | 97.5 | ft/sec |
| Height | 4.5 | ft |
| Stack diameter (top ID) | 4 | inch |
| Stack area | 0.08 | ft ² |

| | | | | |
|------------------------------------|---------|---------------------|-----------------|----------|
| LPG engine output: | 80 | hp | 60.0 | kW |
| LPG engine output: | 0.20 | mmBtu/hr | 1hp=2546 Btu/hr | |
| LPG engine input: | 260.0 | ft ³ /hr | 0.65 | mmBtu/hr |
| Maximum Annual Hours of Operation: | 4000 | hours/year | | |
| Atmospheric Pressure (Ely, NV) | 23.5867 | in Hg | | |

Notes:

¹Particulate matter less than 10 microns aerodynamic (PM₁₀)

² 40 CFR Part 60 Subpart JJJJ, which applies to this unit, is a proposed rule and is not in effect. Should the subpart become a rule, the unit will have to meet certain emission limits, based on its size and type.

Typical heating value commercial-grade propane = 90,500 Btu/gal or 2,500 Btu/ft³

Atmospheric pressure in Ely, NV source: "Useful Tables for Engineers and Steam Users" 11th Edition 1969 - Babcock and Wilcox Company.

A6-10
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
COOLING TOWER EMISSIONS CRITERIA POLLUTANTS

Per Unit (2 Units total)

| <u>Parameter</u> | <u>Units</u> | <u>Scenario 1</u> | <u>Scenario 2</u> | <u>Scenario 3</u> |
|-----------------------------------|--------------------------|-------------------|-------------------|-------------------|
| Ambient Dry Bulb Temp: | ° F | 91 | 44 | 0 |
| Ambient Wet Bulb Temp: | ° F | 61 | 36 | -0.76 |
| Number of cells | # | 24 | 24 | 24 |
| Circulating water flow rate | GPM | 250,000 | 250,000 | 250,000 |
| Exhaust height | ft | 47 | 47 | 47 |
| Exhaust diameter | ft | 32.8 | 32.8 | 32.8 |
| Volume flow rate, total | acfm | 42,803,760 | 42,848,858 | 43,435,471 |
| Volume flow rate, per fan | acfm | 1,188,993 | 1,190,246 | 1,206,541 |
| Exhaust velocity, per fan | fps | 23.45 | 23.48 | 23.80 |
| Exhaust temperature | F | 84.24 | 70.55 | 52.54 |
| Assumed Drift Rate | % of Circ rate | 0.0005% | 0.0005% | 0.0005% |
| Assumed solids content | PPM | 10,000 | 10,000 | 10,000 |
| Water loss due to drift | gpm | 1.25 | 1.25 | 1.25 |
| Water density | lb/gal | 8.34 | 8.34 | 8.34 |
| Pounds of water lost due to drift | lb/min | 10.43 | 10.43 | 10.43 |
| Pounds solids per pound water | lb/lb | 0.01 | 0.01 | 0.01 |
| pounds particulate per minute | lb PM/min | 0.10 | 0.10 | 0.10 |
| pounds per hour - entire tower | lb PM/hr | 6.26 | 6.26 | 6.26 |
| tpy - entire tower | ton PM/yr | 27.40 | 27.40 | 27.40 |
| pounds per hour - per cell | lb PM/hr per cell | 0.26 | 0.26 | 0.26 |

A6-11
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: MCD-1
Source Description: CAR DUMPER DUST COLLECTOR
Pollutants: PM₁₀

Emission Factor From: Manufacturer Guarantee

Explanation: Emissions factor for PM₁₀ for the Car Dumper #1 dust collector is stated by the manufacturers guarantee to be 0.005 grains per dry standard cubic foot.

Emissions are calculated by multiplying the emission factor for PM₁₀ by the maximum flow rating of the baghouse in standard cubic feet per minute. This yields an emissions rate in grains per minute. To generate a short term emission rate in pounds per hour, the calculated emission rate is multiplied by 60 minutes per hour, which is subsequently divided by 7000 grains per pound. To generate an annual emission rate, the short term emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

PM₁₀ Emission Factor = $\frac{0.005 \text{ gr/dscf}}{160,000 \text{ scfm}}$

Short Term Emissions: PM₁₀ in lbs/hr = (baghouse flow rate scfm)*(0.005 gr/dscf)/(7000 gr/lb)*(60 min/hr)

Annual Emissions: PM₁₀ in tons per year = (Short Term PM₁₀)(8760 hr/yr)/(2000 lb/ton)

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-------|------------|-------|
| (TPY) | (g/s) | lb/hr | g/s |
| 30.0 | 0.864 | 6.86 | 0.864 |

Source Name: MCD-2
Source Description: Transfer Tower #1 Dust Collector
Pollutants: PM10

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EMISSIONS CALCULATIONS

Source Name: MCD-4
Source Description: Crusher Building Dust Collector
Pollutants: PM10

Emission Factor From: Manufacturer Guarantee

Explanation: Emissions factor for PM₁₀ for Crusher House dust collector is stated by the manufacturers guarantee to be 0.005 grains per dry standard cubic foot.

Emissions are calculated by multiplying the emission factor for PM10 by the maximum flow rating of the baghouse in standard cubic feet per minute. This yields an emissions rate in grains per minute. To generate a short term emission rate in pounds per hour, the calculated emission rate is multiplied by 60 minutes per hour, which is subsequently divided by 7000 grains per pound. To generate an annual emission rate, the short term emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

PM₁₀ Emission Factor = $\frac{0.005 \text{ gr/dscf}}{23,000 \text{ scfm}}$

Short Term Emissions: PM₁₀ in lbs/hr = (baghouse flow rate scfm)*(0.005 gr/dscf)/(7000 gr/lb)*(60 min/hr)

Annual Emissions: PM₁₀ in tons per year = (Short Term PM₁₀)(8760 hr/yr)/(2000 lb/ton)

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-------|------------|-------|
| (TPY) | (g/s) | lb/hr | g/s |
| 4.32 | 0.124 | 0.99 | 0.124 |

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EMISSIONS CALCULATIONS

Source Name: MCD-5
Source Description: Transfer Tower #3 Dust Collector
Pollutants: PM10

Emission Factor From: Manufacturer Guarantee

Explanation: Emissions factor for PM₁₀ for Transfer Tower #3 dust collector is stated by the manufacturers guarantee to be 0.005 grains per dry standard cubic foot.

Emissions are calculated by multiplying the emission factor for PM10 by the maximum flow rating of the baghouse in standard cubic feet per minute. This yields an emissions rate in grains per minute. To generate a short term emission rate in pounds per hour, the calculated emission rate is multiplied by 60 minutes per hour, which is subsequently divided by 7000 grains per pound. To generate an annual emission rate, the short term emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

PM₁₀ Emission Factor = $\frac{0.005 \text{ gr/dscf}}{21,000 \text{ scfm}}$

Short Term Emissions: PM₁₀ in lbs/hr = (baghouse flow rate scfm)*(0.005 gr/dscf)/(7000 gr/lb)*(60 min/hr)

Annual Emissions: PM₁₀ in tons per year = (Short Term PM₁₀)(8760 hr/yr)/(2000 lb/ton)

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-------|------------|-------|
| (TPY) | (g/s) | lb/hr | g/s |
| 3.94 | 0.113 | 0.90 | 0.113 |

| | |
|-----------------------|--|
| Source Name: | CDC-1 |
| Source Description: | Coal Storage Dome #1 Dust Collector (live storage) |
| Pollutants: | PM10 |
| Emission Factor From: | Manufacturer Guarantee |

Emissions are calculated by multiplying the emission factor for PM10 by the maximum flow rating of the baghouse in standard cubic feet per minute. This yields an emissions rate in grains per minute. To generate a short term emission rate in pounds per hour, the calculated emission rate is multiplied by 60 minutes per hour, which is subsequently divided by 7000 grains per pound. To generate an annual emission rate, the short term emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

Annual Emissions: $\text{PM}_{10} \text{ in tons per year} = (\text{Short Term PM}_{10})(8760 \text{ hr/yr})/(2000 \text{ lb/ton})$

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-------|------------|-------|
| (TPY) | (g/s) | lb/hr | g/s |
| 28.16 | 0.810 | 6.43 | 0.810 |

| | |
|-----------------------|--|
| Source Name: | CDC-2 |
| Source Description: | Coal Storage Dome #2 Dust Collector (live storage) |
| Pollutants: | PM10 |
| Emission Factor From: | Manufacturer Guarantee |

Emissions are calculated by multiplying the emission factor for PM10 by the maximum flow rating of the baghouse in standard cubic feet per minute. This yields an emissions rate in grains per minute. To generate a short term emission rate in pounds per hour, the calculated emission rate is multiplied by 60 minutes per hour, which is subsequently divided by 7000 grains per pound. To generate an annual emission rate, the short term emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

Annual Emissions: $\text{PM}_{10} \text{ in tons per year} = (\text{Short Term PM}_{10})(8760 \text{ hr/yr})/(2000 \text{ lb/ton})$

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-------|------------|-------|
| (TPY) | (g/s) | lb/hr | g/s |
| 28.16 | 0.810 | 6.43 | 0.810 |

Source Name: CDC-3
Source Description: Coal Reclaim Conveyor and Tunnel #1 Dust Collector
Pollutants: PM10

| | |
|---------------------|--|
| Source Name: | CDC-4 |
| Source Description: | Coal Reclaim Conveyor and Tunnel #2 Dust Collector |
| Pollutants: | PM10 |

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EMISSIONS CALCULATIONS

Source Name: CDC-5
Source Description: Coal Tripper Floor Unit #1 Dust Collector A
Pollutants: PM10

Emission Factor From: Manufacturer Guarantee

Explanation: Emissions factor for PM₁₀ for Unit #1 Tripper Bay Dust Collector A is stated by the manufacturers guarantee to be 0.005 grains per dry standard cubic foot.

Emissions are calculated by multiplying the emission factor for PM10 by the maximum flow rating of the baghouse in standard cubic feet per minute. This yields an emissions rate in grains per minute. To generate a short term emission rate in pounds per hour, the calculated emission rate is multiplied by 60 minutes per hour, which is subsequently divided by 7000 grains per pound. To generate an annual emission rate, the short term emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

PM₁₀ Emission Factor = $\frac{0.005 \text{ gr/dscf}}{23,000 \text{ scfm}}$

Short Term Emissions: PM₁₀ in lbs/hr = (baghouse flow rate scfm)*(0.005 gr/dscf)/(7000 gr/lb)*(60 min/hr)

Annual Emissions: PM₁₀ in tons per year = (Short Term PM₁₀)(8760 hr/yr)/(2000 lb/ton)

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-------|------------|-------|
| (TPY) | (g/s) | lb/hr | g/s |
| 4.32 | 0.124 | 0.99 | 0.124 |

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EMISSIONS CALCULATIONS

Source Name: CDC-7
Source Description: Coal Tripper Floor Unit #2 Dust Collector A
Pollutants: PM10

Emission Factor From: Manufacturer Guarantee

Explanation: Emissions factor for PM₁₀ for Unit #2 Tripper Bay Dust Collector A is stated by the manufacturers guarantee to be 0.005 grains per dry standard cubic foot.

Emissions are calculated by multiplying the emission factor for PM10 by the maximum flow rating of the baghouse in standard cubic feet per minute. This yields an emissions rate in grains per minute. To generate a short term emission rate in pounds per hour, the calculated emission rate is multiplied by 60 minutes per hour, which is subsequently divided by 7000 grains per pound. To generate an annual emission rate, the short term emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

PM₁₀ Emission Factor = $\frac{0.005 \text{ gr/dscf}}{23,000 \text{ scfm}}$

Short Term Emissions: PM₁₀ in lbs/hr = (baghouse flow rate scfm)*(0.005 gr/dscf)/(7000 gr/lb)*(60 min/hr)

Annual Emissions: PM₁₀ in tons per year = (Short Term PM₁₀)(8760 hr/yr)/(2000 lb/ton)

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-------|------------|-------|
| (TPY) | (g/s) | lb/hr | g/s |
| 4.32 | 0.124 | 0.99 | 0.124 |

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SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: CH-1
Source Description: Coal Unloading Belt Feeder Transfer Point
Pollutants: PM₁₀

Emission Factor From: AP-42, Section 13.2.4
 "Aggregate Handling and Storage Piles"

Emission Factor Rating: A

Explanation: The emissions factor for PM₁₀ for the coal unloading belt feeder is calculated by using the predictive emission equation specified in Section 13.2.4, Equation (1) in units of pounds per ton. This equation states that the emissions factor of PM₁₀ can be calculated by multiplying the Aerodynamic Particle Size Multiplier of 0.35 (for PM₁₀) by 0.0032. This result is multiplied by the quantity of the mean wind speed divided by 5 and raised to the power of 1.3, with this quantity divided by the quantity of the material moisture content divided by 2 and raised to the power of 1.4. The product of the multiplication specified by Equation (1) is the emission factor in pounds per ton of material processed in a batch drop operation.

The mean wind speed used was the average wind speed for the 1986 - 1990 period for the Ely, NV meteorological station.

Emissions are calculated by multiplying the emission factor for PM₁₀ by the amount of coal loaded per hour, multiplied by 1 minus the control efficiency in percentage. This yields a short term emission rate in pounds per hour. To generate an annual emission rate, the calculated emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

Emission Equations: $E = k * 0.0032 * [(U/5)^{1.3} / ((M/2)^{1.4})]$ lbs/ton Equation (1)
 PM₁₀ emissions = E*(coal loaded)*(1-C) lb/hr Equation (2)

Where: E is the emission factor
 k is the Aerodynamic Particle Size Multiplier (dimensionless)
 U is the mean wind speed in mile per hour
 M is the material moisture content in percent

Data: U = 2.00 mph; set to account for underground conditions
 M = 27 % - material moisture content
 k = 0.35 Aerodynamic Particle Size Multiplier
 C = 100% - controlled via dust collector associated with MDC-1

PM₁₀ Emission Factor = 0.0000089 lbs/ton
 4000 tons/hr

Short Term Emissions: PM₁₀ in lbs/hr =
 (0.35)*(0.0032)*[(9.8/5)^{1.3}]/((29/2)^{1.4})*(tons coal loaded per hour)*(1-1.00)

Annual Emissions: PM₁₀ in tons per year =
 (0.35)*(0.0032)*[(9.8/5)^{1.3}]/((29/2)^{1.4})*(tons coal loaded per hour)*(8760 hr/yr)/(2000 lb/ton)*(1-1.00)

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|---------|------------|---------|
| (TPY) | (g/s) | lb/hr | g/s |
| 0.000 | 0.00000 | 0.0000 | 0.00000 |

Emissions controlled via MDC-1

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SIERRA PACIFIC POWER COMPANY
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EMISSIONS CALCULATIONS

Source Name: CH-2
Source Description: Coal Stockout Conveyor
Pollutants: PM₁₀

Emission Factor From: AP-42, Section 13.2.4
 "Aggregate Handling and Storage Piles"

Emission Factor Rating: A

Explanation: The emissions factor for PM₁₀ for coal stockout is calculated by using the predictive emission equation specified in Section 13.2.4, Equation (1) in units of pounds per ton. This equation states that the emissions factor of PM₁₀ can be calculated by multiplying the Aerodynamic Particle Size Multiplier of 0.35 (for PM₁₀) by 0.0032. This result is multiplied by the quantity of the mean wind speed divided by 5 and raised to the power of 1.3, with this quantity divided by the quantity of the material moisture content divided by 2 and raised to the power of 1.4. The product of the multiplication specified by Equation (1) is the emission factor in pounds per ton of material processed in a batch drop operation.

The mean wind speed used was the average wind speed for the 1986 - 1990 period for the Ely, NV meteorological station.

Emissions are calculated by multiplying the emission factor for PM₁₀ by the amount of coal loaded per hour, multiplied by 1 minus the control efficiency in percentage. This yields a short term emission rate in pounds per hour. To generate an annual emission rate, the calculated emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

Emission Equations: $E = k * 0.0032 * [(U/5)^{1.3} / ((M/2)^{1.4})]$ **lb/ton** **Equation (1)**
 $PM_{10} \text{ emissions} = E * (\text{coal loaded}) * (1 - C)$ **lb/hr** **Equation (2)**

Where: E is the emission factor
 k is the Aerodynamic Particle Size Multiplier (dimensionless)
 U is the mean wind speed in mile per hour
 M is the material moisture content in percent

Data: U = 9.80 mph - 1989 - 1990 Ely, NV mean wind speed
 M = 27 % - material moisture content
 k = 0.35 Aerodynamic Particle Size Multiplier
 C = 75% - control efficiency for telescoping chute

PM₁₀ Emission Factor = 0.0000703 lbs/ton
 4000 tons/hr

Short Term Emissions: PM₁₀ in lbs/hr =
 $(0.35) * (0.0032) * [(9.8/5)^{1.3} / ((27/2)^{1.4})] * (\text{tons coal loaded per hour}) * (1 - 0.75)$

Annual Emissions: PM₁₀ in tons per year =
 $(0.35) * (0.0032) * [(9.8/5)^{1.3} / ((27/2)^{1.4})] * (\text{tons coal loaded per hour}) * (8760 \text{ hr/yr}) / (2000 \text{ lb/ton}) * (1 - 0.75)$

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|--------|------------|--------|
| (TPY) | (g/s) | lb/hr | g/s |
| 0.308 | 0.0089 | 0.070 | 0.0089 |

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SIERRA PACIFIC POWER COMPANY
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EMISSIONS CALCULATIONS

Source Name: CH-3

Source Description: Active Coal Pile Wind Erosion and Maintenance

Pollutants: PM₁₀

Emission Factor From: AP-42, TABLE 11.9-1

"Emission Factor Equations for Uncontrolled Open Dust Sources at Western Surface Coal Mines"

AP-42, Section 13.2.4

"Aggregate Handling and Storage Piles"

Emission Factor Rating: C (Rating applicable to N.W. CO, S.W. CO, and N.E. WY surface sub-bituminous coal mines)

Explanation: Emissions for PM₁₀ from active storage pile wind erosion and maintenance is calculated from the emission factor for Total Suspended Particulate (TSP) provided in Table 11.9-1 and multiplying that value by the average wind speed and the Aerodynamic Particle Size Multiplier for PM₁₀ from Section 13.2.4.

The mean wind speed used was the average wind speed for the 1986 - 1990 period for the Ely, NV meteorological station. This multiplication yields an emission rate in pounds per acre-hour.

Emissions are calculated by multiplying the emission factor for PM₁₀ by the total acreage of the area of disturbance, multiplied by 1 minus the control efficiency in percentage. This yields a short term emission rate in pounds per hour. To generate an annual emission rate, the calculated emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

Emission Equations:

| | | |
|-------------------------|---------------------|--------------------|
| TSP: | E = 0.72*u | lbs/acre-hr |
| PM₁₀: | E = 0.72*u*k | lbs/acre-hr |

Where: E is the emission factor
u is the average wind speed (mph)

Data:

| | |
|------------|--|
| u = | 9.8 mph - 1989 - 1990 Ely, NV mean wind speed |
| k = | 0.35 Aerodynamic Particle Size Multiplier for PM₁₀ |
| C = | 75% control efficiency assumed |
| A = | 3.15 total acreage of area of disturbance |

Short Term Emissions: PM₁₀ in lbs/hr = (0.72)*(9.8 mph)*(0.35)*(total acreage disturbed)*(1-0.90)

Annual Emissions: PM₁₀ in tons per year = (Short Term PM₁₀)(8760 hr/yr)/(2000 lb/ton)

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|----------|------------|----------|
| TPY | g/s | lb/hr | g/s |
| 8.51 | 2.45E-01 | 1.94 | 2.45E-01 |

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EMISSIONS CALCULATIONS

Source Name: CH-4
Emission Source: INACTIVE COAL PILE WIND EROSION
Pollutants: PM₁₀

Emission Factor From: AP-42, Section 13.2.5
 "Industrial Wind Erosion"

Emission Factor Rating: NA

Explanation: Emissions for PM₁₀ from wind erosion of undisturbed area sources is calculated based on the Predictive Emission Factor Equation (Equation 2 in AP-42, Section 13.2.5). This equation relies on the calculation of the erosion potential function for a dry, exposed surface, which in turn relies on the estimation of friction velocity and threshold friction velocity of the disturbed surface. Friction velocity is calculated based on the fastest mile of the reference anemometer for the period between disturbances. The series of required calculations are shown below.

This multiplication yields an emission rate in grams per square meter.

Emission Equations: PM₁₀: $E = k \cdot N \cdot P$ (g/m²)

Where: E is the emission factor
 k is the Aerodynamic Particle Size Multiplier (dimensionless)
 N is the number of disturbances per year
 P is the erosion potential corresponding to the observed fastest mile of wind for the period between disturbances (calculated)

Data: k = 0.5 Aerodynamic Particle Size Multiplier for PM < 10 mm
 N = 1 One disturbance per year assumed for short term modeling

$$P = 58 (u^* - u_t^*)^2 + 25(u^* - u_t^*)$$

Where: P is the erosion potential corresponding to the observed fastest mile of wind for the period between disturbances
 u* is the friction velocity (calculated)
 u_t* is the threshold velocity found in AP-42, Table 13.2.5-2

Data: u_t* = 1.12 Threshold Friction Velocity (m/s) in AP-42 Table 13.2.5-2 for "Uncrusted coal pile"

$$u^* = 0.10 \cdot u_s / u_r \cdot u_{10}$$

Where: u* is the friction velocity
 u_s/u_r is the ratio of surface wind speed to approach wind speed, and is conservatively assumed to equal 0.6 for the entire pile (ref. Figure 13.2.5-2)
 u₁₀ is the fastest mile of reference anemometer for period between disturbances (calculated) (m/s)

$$u_{10} = u \cdot (\ln(10/0.005) / \ln(H_{an}/0.005))$$

Data: u = 18.6 Fastest mile at the Ely, NV meteorological station for the period 1986 - 1990 (m/s)
 H_{an} = 6.1 Anemometer height (m)

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 EMISSIONS CALCULATIONS**

Calculated Values

$u_{10} = 19.9 \text{ (m/s)}$
 $u^* = 1.20 \text{ (m/s)}$
 $P = 2.22 \text{ (g/m}^2\text{)}$
 $E = 1.11 \text{ (g/m}^2\text{/yr)}$

Data:

$A = 185800.0 \text{ undisturbed, exposed area (m}^2\text{)}$
 $C = 50.0\% \text{ percent control efficiency for compaction}$

Short Term Emissions: $PM_{10} \text{ in lbs/hr} = (1.11) * (\text{total undisturbed area}) * (1 - 0.90)$

Annual Emissions: $PM_{10} \text{ in tons per year} = (\text{Short Term } PM_{10}) * (8760 \text{ hr/yr}) / (2000 \text{ lb/ton})$

| Annual PM_{10} EMISSIONS | | Short Term | |
|----------------------------|----------|------------|----------|
| TPY | g/s | lb/hr | g/s |
| 0.11 | 3.27E-03 | 0.026 | 3.27E-03 |

| | |
|---------------------|---------------------------------|
| Source Name: | LDC-2 |
| Source Description: | Limestone Silo A Dust Collector |
| Pollutants: | PM10 |

Explanation: Emissions factor for PM10 for the Limestone Silo A dust collector is stated by the manufacturers guarantee to be 0.01 grains per dry standard cubic foot.

| | | |
|------------------------------------|------|---------|
| PM ₁₀ Emission Factor = | 0.01 | gr/dscf |
| | 700 | scfm |

Annual Emissions: $\text{PM}_{10} \text{ in tons per year} = (\text{Short Term PM}_{10})(8760 \text{ hr/yr})/(2000 \text{ lb/ton})$

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-----------|------------|----------|
| (TPY) | (g/s) | lb/hr | g/s |
| 0.263 | 0.0075599 | 0.060 | 0.007560 |

| | |
|---------------------|---------------------------------|
| Source Name: | LDC-3 |
| Source Description: | Limestone Silo B Dust Collector |
| Pollutants: | PM10 |

Explanation: Emissions factor for PM10 for the Limestone Silo B dust collector is stated by the manufacturers guarantee to be 0.01 grains per dry standard cubic foot.

| | | |
|------------------------------------|------|---------|
| PM ₁₀ Emission Factor = | 0.01 | gr/dscf |
| | 700 | scfm |

Annual Emissions: $\text{PM}_{10} \text{ in tons per year} = (\text{Short Term PM}_{10})(8760 \text{ hr/yr})/(2000 \text{ lb/ton})$

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-----------|------------|----------|
| (TPY) | (g/s) | lb/hr | g/s |
| 0.263 | 0.0075599 | 0.060 | 0.007560 |

| | |
|----------------------------|--|
| Source Name: | LDC-4 |
| Source Description: | Limestone Reclaim Tunnel Dust Collector |
| Pollutants: | PM10 |

| | |
|---------------------|---|
| Source Name: | LDC-5 |
| Source Description: | Limestone Unloading Building Dust Collector |
| Pollutants: | PM10 |

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EMISSIONS CALCULATIONS

Source Name: LH-1
Source Description: Limestone Unloading Conveyor Transfer Point
Pollutants: PM₁₀

Emission Factor From: AP-42, Section 13.2.4
 "Aggregate Handling and Storage Piles"

Emission Factor Rating: A

Explanation:

The emissions factor for PM₁₀ for limestone unloading conveyor is calculated by using the predictive emission equation specified in Section 13.2.4, Equation (1) in units of pounds per ton. This equation states that emissions factor of PM10 can be calculated by multiplying the Aerodynamic Particle Size Multiplier provided in the text by 0.0032. This result is multiplied by the quantity of the mean wind speed divided by 5 and raised to the power of 1.3, with this quantity divided by the quantity of the material moisture content divided by 2 and raised to the power of 1.4. The product of the multiplication specified by Equation (1) is the emission factor in pounds per ton of material processed in a batch drop operation.

The mean wind speed used was the site specific mean wind speed.

Emissions are calculated by multiplying the emission factor for PM10 by the amount of limestone loaded per hour, multiplied by 1 minus the control efficiency in percentage. This yields a short term emission rate in pounds per hour. To generate an annual emission rate, the calculated emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

Emission Equations: $E = k * 0.0032 * [(U/5)^{1.3} / ((M/2)^{1.4})]$ lbs/ton Equation (1)
 PM₁₀ emissions = E*(coal loaded)*(1-C) lb/hr Equation (2)

Where: E is the emission factor
 k is the Aerodynamic Particle Size Multiplier (dimensionless)
 U is the mean wind speed in mile per hour
 M is the material moisture content in percent

Data: U = 9.80 mph - mean wind speed
 M = 4.00 % - material moisture content
 k = 0.35 Aerodynamic Particle Size Multiplier
 C = 80% - control efficiency for fines screening in lowering well

PM₁₀ Emission Factor = 0.001 lbs/ton
 600 tons/hr

Short Term Emissions: PM₁₀ in lbs/hr =
 (0.35)(0.0032)[((9.8/5)^{1.3})/((4/2)^{1.4}](tons limestone loaded per hour)(1-0.80)

Annual Emissions: PM₁₀ in tons per year =
 (0.35)(0.0032)[((9.8/5)^{1.3})/((4/2)^{1.4}][(tons limestone loaded per hour)(8760 hr/yr)/(2000 lb/ton)](1-0.80)

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-----------|------------|----------|
| (TPY) | (g/s) | lb/hr | g/s |
| 0.535 | 0.0153905 | 0.122 | 0.015391 |

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SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: LH-2
Source Description: Limestone Silo A Loading Conveyor Transfer Point
Pollutants: PM₁₀

Emission Factor From: AP-42, Section 13.2.4
 "Aggregate Handling and Storage Piles"

Emission Factor Rating: A

Explanation: The emissions factor for PM₁₀ for limestone silo A loading conveyor transfer point is calculated by using the predictive emission equation specified in Section 13.2.4, Equation (1) in units of pounds per ton. This equation states that emissions factor of PM10 can be calculated by multiplying the Aerodynamic Particle Size Multiplier provided in the text by 0.0032. This result is multiplied by the quantity of the mean wind speed divided by 5 and raised to the power of 1.3, with this quantity divided by the quantity of the material moisture content divided by 2 and raised to the power of 1.4. The product of the multiplication specified by Equation (1) is the emission factor in pounds per ton of material processed in a batch drop operation.

The mean wind speed used was the site specific mean wind speed.

Emissions are calculated by multiplying the emission factor for PM10 by the amount of limestone loaded per hour, multiplied by 1 minus the control efficiency in percentage. This yields a short term emission rate in pounds per hour. To generate an annual emission rate, the calculated emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

Emission Equations: $E = k * 0.0032 * [((U/5)^{1.3}) / ((M/2)^{1.4})]$ **lbs/ton** **Equation (1)**
 $PM_{10} \text{ emissions} = E * (\text{coal loaded}) * (1 - C)$ **lb/hr** **Equation (2)**

Where: E is the emission factor
 k is the Aerodynamic Particle Size Multiplier (dimensionless)
 U is the mean wind speed in mile per hour
 M is the material moisture content in percent

Data: U = 2.00 mph - mean wind speed for enclosed conditions
 M = 4.00 % - material moisture content
 k = 0.35 Aerodynamic Particle Size Multiplier
 C = 50% - control efficiency for enclosure

PM₁₀ Emission Factor = 0.0001 lbs/ton
 600 tons/hr

Short Term Emissions: PM₁₀ in lbs/hr =
 (0.35)(0.0032)[((9.8/5)^{1.3})/((4/2)^{1.4}](tons limestone loaded per hour)(1-0.50)

Annual Emissions: PM₁₀ in tons per year =
 (0.35)(0.0032)[((9.8/5)^{1.3})/((4/2)^{1.4}][(tons limestone loaded per hour)(8760 hr/yr)/(2000 lb/ton)](1-0.50)

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-----------|------------|----------|
| (TPY) | (g/s) | lb/hr | g/s |
| 0.169 | 0.0048746 | 0.039 | 0.004875 |

A6-35
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: LH-3
Source Description: Limestone Silo B Loading Conveyor Transfer Point
Pollutants: PM₁₀

Emission Factor From: AP-42, Section 13.2.4
 "Aggregate Handling and Storage Piles"

Emission Factor Rating: A

Explanation: The emissions factor for PM₁₀ for limestone silo B loading conveyor transfer point is calculated by using the predictive emission equation specified in Section 13.2.4, Equation (1) in units of pounds per ton. This equation states that emissions factor of PM10 can be calculated by multiplying the Aerodynamic Particle Size Multiplier provided in the text by 0.0032. This result is multiplied by the quantity of the mean wind speed divided by 5 and raised to the power of 1.3, with this quantity divided by the quantity of the material moisture content divided by 2 and raised to the power of 1.4. The product of the multiplication specified by Equation (1) is the emission factor in pounds per ton of material processed in a batch drop operation

The mean wind speed used was the site specific mean wind speed.

Emissions are calculated by multiplying the emission factor for PM10 by the amount of limestone loaded per hour, multiplied by 1 minus the control efficiency in percentage. This yields a short term emission rate in pounds per hour. To generate an annual emission rate, the calculated emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

Emission Equations: $E = k \cdot 0.0032 \cdot [(U/5)^{1.3} / ((M/2)^{1.4})]$ lbs/ton Equation (1)
 PM₁₀ emissions = E*(coal loaded)*(1-C) lb/hr Equation (2)

Where: E is the emission factor
 k is the Aerodynamic Particle Size Multiplier (dimensionless)
 U is the mean wind speed in mile per hour
 M is the material moisture content in percent

Data: U = 2.00 mph - mean wind speed for enclosed conditions
 M = 4.00 % - material moisture content
 k = 0.35 Aerodynamic Particle Size Multiplier
 C = 50% - control efficiency for enclosure

PM₁₀ Emission Factor = 0.000 lbs/ton
 600 tons/hr

Short Term Emissions: PM₁₀ in lbs/hr =
 (0.35)(0.0032)[((9.8/5)^{1.3})/((4/2)^{1.4}](tons limestone loaded per hour)(1-0.50)

Annual Emissions: PM₁₀ in tons per year =
 (0.35)(0.0032)[((9.8/5)^{1.3})/((4/2)^{1.4}][(tons limestone loaded per hour)(8760 hr/yr)/(2000 lb/ton)](1-0.50)

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-----------|------------|----------|
| (TPY) | (g/s) | lb/hr | g/s |
| 0.169 | 0.0048746 | 0.039 | 0.004875 |

A6-36
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: LH-4
Source Description: Limestone Pile Wind Erosion and Maintenance
Pollutants: PM₁₀

Emission Factor From: AP-42, TABLE 11.9-1
 "Emission Factor Equations for Uncontrolled Open Dust Sources at Western Surface Coal Mines"
 AP-42, Section 13.2.4
 "Aggregate Handling and Storage Piles"

Emission Factor Rating: C (Rating applicable to N.W. CO, S.W. CO, and N.E. WY surface sub-bituminous coal mines)

Explanation: Emissions for PM₁₀ from active storage pile wind erosion and maintenance is calculated from the emission factor for Total Suspended Particulate (TSP) provided in Table 11.9-1 and multiplying that value by the average wind speed and the Aerodynamic Particle Size Multiplier for PM₁₀ from Section 13.2.4.

The mean wind speed used was the average wind speed for the 1986 - 1990 period for the Ely, NV meteorological station. This multiplication yields an emission rate in pounds per acre-hour.

Emissions are calculated by multiplying the emission factor for PM₁₀ by the total acreage of the area of disturbance, multiplied by 1 minus the control efficiency in percentage. This yields a short term emission rate in pounds per hour. To generate an annual emission rate, the calculated emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

Emission Equations:

| | | |
|-------------------------|--------------------|-------------|
| TSP: | $E = 0.72 * u$ | lbs/acre-hr |
| PM₁₀: | $E = 0.72 * u * k$ | lbs/acre-hr |

Where: E is the emission factor
 u is the average wind speed (mph)

Data:

| | |
|------------|--|
| u = | 9.8 mph - 1989 - 1990 Ely, NV mean wind speed |
| k = | 0.35 Aerodynamic Particle Size Multiplier for PM₁₀ |
| C = | 0% no control efficiency assumed |
| A = | 0.56 total acreage of area of disturbance |

Short Term Emissions: PM₁₀ in lbs/hr = (0.72)*(9.8 mph)*(0.35)*(total acreage disturbed)*(1-0.0)

Annual Emissions: PM₁₀ in tons per year = (Short Term PM₁₀)(8760 hr/yr)/(2000 lb/ton)

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|----------|------------|----------|
| TPY | g/s | lb/hr | g/s |
| 6.07 | 1.75E-01 | 1.39 | 1.75E-01 |

| | |
|----------------------------|---------------------------------------|
| Source Name: | ACD-1 |
| Source Description: | Fly Ash Silo #1 Dust Collector |
| Pollutants: | PM10 |

| | |
|----------------------------|---------------------------------------|
| Source Name: | ACD-2 |
| Source Description: | Fly Ash Silo #2 Dust Collector |
| Pollutants: | PM10 |

| | |
|----------------------------|---|
| Source Name: | ACD-3 |
| Source Description: | Bottom Ash Silo 1 Dust Collector |
| Pollutants: | PM10 |

Explanation: Emissions factor for PM10 for the Bottom Ash Silo 1 dust collector is stated by the manufacturers guarantee to be 0.01 grains per dry standard cubic foot.

| | | |
|------------------------------------|-------|---------|
| PM ₁₀ Emission Factor = | 0.01 | gr/dscf |
| | 1,000 | scfm |

Annual Emissions: $\text{PM}_{10} \text{ in tons per year} = (\text{Short Term PM}_{10})(8760 \text{ hr/yr})/(2000 \text{ lb/ton})$

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-----------|------------|----------|
| (TPY) | (g/s) | lb/hr | g/s |
| 0.375 | 0.0107998 | 0.086 | 0.010800 |

| | |
|----------------------------|---|
| Source Name: | ACD-4 |
| Source Description: | Bottom Ash Silo 2 Dust Collector |
| Pollutants: | PM10 |

A6-41
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: GH-1
Source Description: Gypsum Stockout Conveyor
Pollutants: PM₁₀

Emission Factor From: AP-42, Section 13.2.4
 "Aggregate Handling and Storage Piles"

Emission Factor Rating: A

Explanation: The emissions factor for PM10 for the gypsum stockout conveyor is calculated by using the predictive emission equation specified in Section 13.2.4, Equation (1) in units of pounds per ton. This equation states that emissions factor of PM10 can be calculated by multiplying the Aerodynamic Particle Size Multiplier provided in the text by 0.0032. This result is multiplied by the quantity of the mean wind speed divided by 5 and raised to the power of 1.3, with this quantity divided by the quantity of the material moisture content divided by 2 and raised to the power of 1.4. The product of the multiplication specified by Equation (1) is the emission factor in pounds per ton of material processed in a batch drop operation.

The mean wind speed used was the site specific mean wind speed.

Emissions are calculated by multiplying the emission factor for PM10 by the amount of gypsum loaded per hour. This yields a short term emission rate in pounds per hour. To generate an annual emission rate, the calculated emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

Emission Equations: $E = k * 0.0032 * [(U/5)^{1.3} / ((M/2)^{1.4})]$ lbs/ton Equation (1)
 PM₁₀ emissions = E*(coal loaded)*(1-C) lb/hr Equation (2)

Where: E is the emission factor
 k is the Aerodynamic Particle Size Multiplier (dimensionless)
 U is the mean wind speed in mile per hour
 M is the material moisture content in percent

Data: U = 9.80 mph - mean wind speed
 M = 10.00 % - material moisture content
 k = 0.35 Aerodynamic Particle Size Multiplier

PM₁₀ Emission Factor = 0.0002822 lbs/ton
 400 tons/hr

Short Term Emissions: PM₁₀ in lbs/hr =
 (0.35)(0.0032)[((9.8/5)^{1.3})/((10/2)^{1.4}](tons gypsum loaded per hour)

Annual Emissions: PM₁₀ in tons per year =
 (0.35)(0.0032)[((9.8/5)^{1.3})/((10/2)^{1.4}][(tons gypsum loaded per hour)(8760 hr/yr)/(2000 lb/ton)]

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-----------|------------|----------|
| (TPY) | (g/s) | lb/hr | g/s |
| 0.494 | 0.0142238 | 0.113 | 0.014224 |

A6-42
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: GH-2
Source Description: Gypsum Pile Wind Erosion and Maintenance
Pollutants: PM₁₀

Emission Factor From: AP-42, TABLE 11.9-1
 "Emission Factor Equations for Uncontrolled Open Dust Sources at Western Surface Coal Mines"
 AP-42, Section 13.2.4
 "Aggregate Handling and Storage Piles"

Emission Factor Rating: C (Rating applicable to N.W. CO, S.W. CO, and N.E. WY surface sub-bituminous coal mines)

Explanation: Emissions for PM₁₀ from active storage pile wind erosion and maintenance is calculated from the emission factor for Total Suspended Particulate (TSP) provided in Table 11.9-1 and multiplying that value by the average wind speed and the Aerodynamic Particle Size Multiplier for PM₁₀ from Section 13.2.4.

The mean wind speed used was the average wind speed for the 1986 - 1990 period for the Ely, NV meteorological station. This multiplication yields an emission rate in pounds per acre-hour.

Emissions are calculated by multiplying the emission factor for PM₁₀ by the total acreage of the area of disturbance, multiplied by 1 minus the control efficiency in percentage. This yields a short term emission rate in pounds per hour. To generate an annual emission rate, the calculated emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

Emission Equations: TSP: $E = 0.72 * u$ lbs/acre-hr
 PM₁₀: $E = 0.72 * u * k$ lbs/acre-hr

Where: E is the emission factor
 u is the average wind speed (mph)

Data: u = 9.8 mph - 1989 - 1990 Ely, NV mean wind speed
 k = 0.35 Aerodynamic Particle Size Multiplier for PM₁₀
 C = 75% control efficiency assumed associated with 3-sided enclosure
 A = 0.33 total acreage of area of disturbance

Short Term Emissions: PM₁₀ in lbs/hr = $(0.72) * (9.8 \text{ mph}) * (0.35) * (\text{total acreage disturbed}) * (1 - 0.75)$

Annual Emissions: PM₁₀ in tons per year = $(\text{Short Term PM}_{10}) * (8760 \text{ hr/yr}) / (2000 \text{ lb/ton})$

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|----------|------------|----------|
| TPY | g/s | lb/hr | g/s |
| 0.91 | 2.61E-02 | 0.21 | 2.61E-02 |

| | |
|---------------------|--|
| Source Name: | IDC-2 |
| Source Description: | PAC Storage Silo Unit 1 Dust Collector |
| Pollutants: | PM10 |

| | |
|----------------------------|---|
| Source Name: | IDC-3 |
| Source Description: | DSI Storage Silo Unit 2 Dust Collector |
| Pollutants: | PM10 |

Explanation: Emissions factor for PM10 for the DSI Storage Silo Unit 2 dust collector is stated by the manufacturers guarantee to be 0.01 grains per dry standard cubic foot.

| | | |
|------------------------------------|------|---------|
| PM ₁₀ Emission Factor = | 0.01 | gr/dscf |
| | 600 | scfm |

Annual Emissions: $\text{PM}_{10} \text{ in tons per year} = (\text{Short Term PM}_{10})(8760 \text{ hr/yr})/(2000 \text{ lb/ton})$

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-----------|------------|----------|
| (TPY) | (g/s) | lb/hr | g/s |
| 0.225 | 0.0064799 | 0.051 | 0.006480 |

| | |
|---------------------|--|
| Source Name: | IDC-4 |
| Source Description: | PAC Storage Silo Unit 2 Dust Collector |
| Pollutants: | PM10 |

Explanation: Emissions factor for PM10 for the PAC Storage Silo Unit 2 dust collector is stated by the manufacturers guarantee to be 0.01 grains per dry standard cubic foot.

| | | |
|------------------------------------|------|---------|
| PM ₁₀ Emission Factor = | 0.01 | gr/dscf |
| | 600 | scfm |

Annual Emissions: $\text{PM}_{10} \text{ in tons per year} = (\text{Short Term PM}_{10})(8760 \text{ hr/yr})/(2000 \text{ lb/ton})$

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-----------|------------|----------|
| (TPY) | (g/s) | lb/hr | g/s |
| 0.225 | 0.0064799 | 0.051 | 0.006480 |

| | |
|----------------------------|---|
| Source Name: | WDC-2 |
| Source Description: | Lime Storage Silo Dust Collector |
| Pollutants: | PM10 |

Explanation: Emissions factor for PM10 for the Lime Storage Silo dust collector is stated by the manufacturers guarantee to be 0.01 grains per dry standard cubic foot.

| | | |
|------------------------------------|------|---------|
| PM ₁₀ Emission Factor = | 0.01 | gr/dscf |
| | 600 | scfm |

Annual Emissions: $\text{PM}_{10} \text{ in tons per year} = (\text{Short Term PM}_{10})(8760 \text{ hr/yr})/(2000 \text{ lb/ton})$

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-----------|------------|----------|
| (TPY) | (g/s) | lb/hr | g/s |
| 0.225 | 0.0064799 | 0.051 | 0.006480 |

| | |
|-----------------------|---|
| Source Name: | WDC-3 |
| Source Description: | Magnesium Hydroxide Storage Silo Dust Collector |
| Pollutants: | PM10 |
| Emission Factor From: | Manufacturer Guarantee |

Emissions are calculated by multiplying the emission factor for PM10 by the maximum flow rating of the baghouse in standard cubic feet per minute. This yields an emissions rate in grains per minute. To generate a short term emission rate in pounds per hour, the calculated emission rate is multiplied by 60 minutes per hour, which is subsequently divided by 7000 grains per pound. To generate an annual emission rate, the short term emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

Annual Emissions: $\text{PM}_{10} \text{ in tons per year} = (\text{Short Term PM}_{10})(8760 \text{ hr/yr})/(2000 \text{ lb/ton})$

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-----------|------------|----------|
| (TPY) | (g/s) | lb/hr | g/s |
| 0.225 | 0.0064799 | 0.051 | 0.006480 |

A6-50
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: LF-1, LF-2, LF-3
Emission Source: INACTIVE LANDFILL PILE WIND EROSION
Pollutants: PM₁₀

Emission Factor From: AP-42, Section 13.2.5
"Industrial Wind Erosion"

Emission Factor Rating: NA

Explanation:

Emissions for PM₁₀ from wind erosion of undisturbed area sources is calculated based on the Predictive Emission Factor Equation (Equation 2 in AP-42, Section 13.2.5). This equation relies on the calculation of the erosion potential function for a dry, exposed surface, which in turn relies on the estimation of friction velocity and threshold friction velocity of the disturbed surface. Because there are no disturbances expected for this exposed surface, no emissions are associated with this source.

Friction velocity is calculated based on the fastest mile of the reference anemometer for the period between disturbances. The series of required calculations are shown below.

This multiplication yields an emission rate in grams per square meter.

Emission Equations: PM₁₀: $E = k \cdot N \cdot P \text{ (g/m}^2\text{)}$

Where: E is the emission factor
k is the Aerodynamic Particle Size Multiplier (dimensionless)
N is the number of disturbances per year
P is the erosion potential corresponding to the observed fastest mile of wind for the period between disturbances (calculated)

Data: k = 0.5 Aerodynamic Particle Size Multiplier for PM < 10 mm
N = 0 No disturbances per year are expected on the inactive portion of the landfill

$$P = 58 (u^* - u_t^*)^2 + 25(u^* - u_t^*)$$

Where: P is the erosion potential corresponding to the observed fastest mile of wind for the period between disturbances
u* is the friction velocity (calculated)
u_t* is the threshold velocity found in AP-42, Table 13.2.5-2

Data: u_t* = 1.02 Threshold Friction Velocity (m/s) in AP-42 Table 13.2.5-2 for "Overburden"

u* = 0.053 * u₁₀ **Note:** This equation is restricted to large relatively flat piles or exposed areas with little penetration into the surface wind layer.

Where: u* is the friction velocity
u₁₀ is the fastest mile of reference anemometer for period between disturbances (calculated) (m/s)
 $u_{10} = u * (\ln(10/0.005)/\ln(H_{an}/0.005))$

Data: u = 18.6 Fastest mile at the Ely, NV meteorological station for the period 1986 - 1990 (m/s)
H_{an} = 6.1 Anemometer height (m)

A6-50
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Calculated Values

$u_{10} = 19.9 \text{ (m/s)}$
 $u^* = 1.06 \text{ (m/s)}$
 $P = 0.98 \text{ (g/m}^2\text{)}$
 $E = 0.000 \text{ (g/m}^2\text{/yr)}$

Data:

Area 1 = 2,141,345 undisturbed, exposed area (m²)
Area 2 = 850,615.6 undisturbed, exposed area (m²)
5 yr cell = 363,283.6 undisturbed, exposed area (m²)
C = 0.0% percent control efficiency

Short Term Emissions: PM_{10} in lbs/hr = (0.49)*(total undisturbed area)

Annual Emissions: PM_{10} in tons per year = (Short Term PM_{10})(8760 hr/yr)/(2000 lb/ton)

| Landfill Area | Source Name | Annual PM_{10} EMISSIONS | | Short Term | |
|---------------|-------------|----------------------------|----------|------------|----------|
| | | TPY | g/s | lb/hr | g/s |
| East Portion | LF-1 | 0.000 | 0.00E+00 | 0.000 | 0.00E+00 |
| West Portion | LF-2 | 0.000 | 0.00E+00 | 0.000 | 0.00E+00 |
| 5-year Cell | LF-3 | 0.000 | 0.00E+00 | 0.000 | 0.00E+00 |

A6-51
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: LF-4
Source Description: Landfill Stockout
Pollutants: PM₁₀

Emission Factor From: AP-42, Section 13.2.4
 "Aggregate Handling and Storage Piles"

Emission Factor Rating: A

Explanation: The emissions factor for PM10 for landfill stockout is calculated by using the predictive emission equation specified in Section 13.2.4, Equation (1) in units of pounds per ton. This equation states that emissions factor of PM10 can be calculated by multiplying the Aerodynamic Particle Size Multiplier provided in the text by 0.0032. This result is multiplied by the quantity of the mean wind speed divided by 5 and raised to the power of 1.3, with this quantity divided by the quantity of the material moisture content divided by 2 and raised to the power of 1.4. The product of the multiplication specified by Equation (1) is the emission factor in pounds per ton of material processed in a batch drop operation.

The mean wind speed used was the site specific mean wind speed.

Emissions are calculated by multiplying the emission factor for PM10 by the amount of landfill material loaded per hour. This yields a short term emission rate in pounds per hour. To generate an annual emission rate, the calculated emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

Emission Equations: $E = k * 0.0032 * [(U/5)^{1.3} / ((M/2)^{1.4})]$ lbs/ton Equation (1)
 PM₁₀ emissions = E*(coal loaded)*(1-C) lb/hr Equation (2)

Where: E is the emission factor
 k is the Aerodynamic Particle Size Multiplier (dimensionless)
 U is the mean wind speed in mile per hour
 M is the material moisture content in percent

Data: U = 9.80 mph - mean wind speed
 M = 10.00 % - material moisture content
 k = 0.35 Aerodynamic Particle Size Multiplier
 C = 90% control efficiency assumed associated with water trucks and crusting expected

PM₁₀ Emission Factor = 0.0000282 lbs/ton
 122 tons/hr

Short Term Emissions: PM₁₀ in lbs/hr =
 (0.35)*(0.0032)*[(9.8/5)^{1.3}]/((10/2)^{1.4})*(tons landfill material loaded per hour)*(1-0.90)

Annual Emissions: PM₁₀ in tons per year =
 (0.35)*(0.0032)*[(9.8/5)^{1.3}]/((10/2)^{1.4})*(tons landfill material loaded per hour)*(1-0.90)*(8760 hr/yr)/(2000 lb/ton)

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|-----------|------------|----------|
| (TPY) | (g/s) | lb/hr | g/s |
| 0.015 | 0.0004338 | 0.003 | 0.000434 |

A6-52
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: LF-5
Source Description: Active Landfill Pile Wind Erosion and Maintenance
Pollutants: PM₁₀

Emission Factor From: AP-42, TABLE 11.9-1
 "Emission Factor Equations for Uncontrolled Open Dust Sources at Western Surface Coal Mines"
 AP-42, Section 13.2.4
 "Aggregate Handling and Storage Piles"

Emission Factor Rating: C (Rating applicable to N.W. CO, S.W. CO, and N.E. WY surface sub-bituminous coal mines)

Explanation: Emissions for PM₁₀ from active storage pile wind erosion and maintenance is calculated from the emission factor for Total Suspended Particulate (TSP) provided in Table 11.9-1 and multiplying that value by the average wind speed and the Aerodynamic Particle Size Multiplier for PM₁₀ from Section 13.2.4.

The mean wind speed used was the average wind speed for the 1986 - 1990 period for the Ely, NV meteorological station. This multiplication yields an emission rate in pounds per acre-hour.

Emissions are calculated by multiplying the emission factor for PM₁₀ by the total acreage of the area of disturbance, multiplied by 1 minus the control efficiency in percentage. This yields a short term emission rate in pounds per hour. To generate an annual emission rate, the calculated emission rate is multiplied by the number of hours of operation per year in which material handling will be performed. This yields an emission rate in pounds per year, which is subsequently divided by 2000 to yield tons per year.

Emission Equations:

| | | |
|-------------------------|--------------------------------------|--------------------|
| TSP: | $E = 0.72 * u$ | lbs/acre-hr |
| PM₁₀: | $E = 0.72 * u * k$ | lbs/acre-hr |

Where: E is the emission factor
 u is the average wind speed (mph)

Data:

| | |
|------------|--|
| u = | 9.8 mph - 1989 - 1990 Ely, NV mean wind speed |
| k = | 0.35 Aerodynamic Particle Size Multiplier for PM₁₀ |
| C = | 90% control efficiency assumed associated with water trucks and crusting expected |
| A = | 9.86 total acreage of area of disturbance |

Short Term Emissions: PM₁₀ in lbs/hr = $(0.72) * (9.8 \text{ mph}) * (0.35) * (\text{total acreage disturbed}) * (1 - 0.90)$

Annual Emissions: PM₁₀ in tons per year = $(\text{Short Term PM}_{10}) * (8760 \text{ hr/yr}) / (2000 \text{ lb/ton})$

| Annual PM ₁₀ EMISSIONS | | Short Term | |
|-----------------------------------|----------|------------|----------|
| TPY | g/s | lb/hr | g/s |
| 10.66 | 3.07E-01 | 2.43 | 3.07E-01 |

A6-53
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
ROAD HAUL EMISSIONS CRITERIA POLLUTANTS

- (a) Paved Road AP-42 Emission Factor (lb/VMT) $E = (k (sL/2)^{0.65} (W/3)^{1.5} - C) * (1-(P/4/N))$
- (b) Unpaved Road AP-42 Emission Factor (lb/VMT) $E = (k (s/12)^a (W/3)^b) * ((365-p)/365)$

Limestone Supply

| | | | |
|--|-------|-------------------|--------------------|
| Average Round Trip Distance | = | 0.0 miles Paved | |
| | = | 3.9 miles Unpaved | |
| Tons per year (m) | = | 11,287.00 tons/yr | |
| tons per truck (n) | = | 20 tons/truck | |
| Trucks per year | = | 564 trucks/yr | loaded |
| Paved Constant PM-10 (lb/VMT) | k = | 0.016 (i) | |
| Paved Constant PM (lb/VMT) | k = | 0.082 (i) | |
| Paved Paved Silt Loading (g/m ²) | sL = | 9.7 (j) | |
| Paved 1980's Vehicle Fleet Emission Factor PM-10 (lb/VMT) | C = | 0.00047 (k) | |
| Paved 1980's Vehicle Fleet Emission Factor PM (lb/VMT) | C = | 0.00047 (k) | |
| Unpaved Constant PM-10 (lb/VMT) | k = | 1.5 (c) | |
| Unpaved Constant PM (lb/VMT) | k = | 4.9 (c) | |
| Unpaved Surface Material Silt Content (%) | s = | 8.4 (d) | |
| Unpaved Constant PM-10 (lb/VMT) | a = | 0.9 (c) | |
| Unpaved Constant PM (lb/VMT) | a = | 0.7 (c) | |
| Unpaved Constant PM-10 (lb/VMT) | b = | 0.45 (c) | |
| Unpaved Constant PM (lb/VMT) | b = | 0.45 (c) | |
| Average Fleet Truck weight (ton) | W = | 33 (e) | |
| Annual days with rain | p = | 73.7 (f) | |
| Number of days in precipitation averaging period | N = | 365 | |
| Paved Road Uncontrolled Emission Factor PM10 (lb/VMT) | E = | 1.5 | |
| Paved Road Uncontrolled Emission Factor PM (lb/VMT) | E = | 7.7 | |
| Unpaved Road Uncontrolled Emission Factor PM10 (lb/VMT) | E = | 2.5 | |
| Unpaved Road Uncontrolled Emission Factor PM (lb/VMT) | E = | 8.9 | |
| Paved Annual Vehicle Miles (VMT) | VMT = | 0 (g) | |
| Unpaved Annual Vehicle Miles (VMT) | VMT = | 2,202 (g) | 6.03367348 VMT/day |
| Unpaved Mg/Cl Control Efficiency and reduce speed | = | 95% (h) | |
| Paved Control Efficiency (vacuum sweeping twice per month) | = | 79% (l) | |
| Controlled PM-10 Paved Road Emissions | = | 0.00 TPY | |
| Controlled PM-10 Unpaved Road Emissions | = | 0.49 TPY | |

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(a) Paved Road AP-42 Emission Factor (lb/VMT) $E = (k (sL/2)^{0.65} (W/3)^{1.5} - C) * (1-(P/4/N))$

(b) Unpaved Road AP-42 Emission Factor (lb/VMT) $E = (k (s/12)^a (W/3)^b) * ((365-p)/365)$

Soda Ash Supply

| | | | |
|--|-------|-------------------|--------|
| Average Round Trip Distance | = | 0.0 miles Paved | |
| | = | 3.9 miles Unpaved | |
| Tons per year (m) | = | 2,190.00 tons/yr | |
| tons per truck (n) | = | 20 tons/truck | |
| Trucks per year | = | 110 trucks/yr | loaded |
| Paved Constant PM-10 (lb/VMT) | k = | 0.016 | (i) |
| Paved Constant PM (lb/VMT) | k = | 0.082 | (i) |
| Paved Paved Silt Loading (g/m ²) | sL = | 9.7 | (j) |
| Paved 1980's Vehicle Fleet Emission Factor PM-10 (lb/VMT) | C = | 0.00047 | (k) |
| Paved 1980's Vehicle Fleet Emission Factor PM (lb/VMT) | C = | 0.00047 | (k) |
| Unpaved Constant PM-10 (lb/VMT) | k = | 1.5 | (c) |
| Unpaved Constant PM (lb/VMT) | k = | 4.9 | (c) |
| Unpaved Surface Material Silt Content (%) | s = | 8.4 | (d) |
| Unpaved Constant PM-10 (lb/VMT) | a = | 0.9 | (c) |
| Unpaved Constant PM (lb/VMT) | a = | 0.7 | (c) |
| Unpaved Constant PM-10 (lb/VMT) | b = | 0.45 | (c) |
| Unpaved Constant PM (lb/VMT) | b = | 0.45 | (c) |
| Average Fleet Truck weight (ton) | W = | 33 | (e) |
| Annual days with rain | p = | 73.7 | (f) |
| Number of days in precipitation averaging period | N = | 365 | |
| Paved Road Uncontrolled Emission Factor PM10 (lb/VMT) | E = | 1.5 | |
| Paved Road Uncontrolled Emission Factor PM (lb/VMT) | E = | 7.7 | |
| Unpaved Road Uncontrolled Emission Factor PM10 (lb/VMT) | E = | 2.5 | |
| Unpaved Road Uncontrolled Emission Factor PM (lb/VMT) | E = | 8.9 | |
| Paved Annual Vehicle Miles (VMT) | VMT = | 0 | (g) |
| Unpaved Annual Vehicle Miles (VMT) | VMT = | 427 | (g) |
| Unpaved Mg/Ci Control Efficiency and reduce speed | = | 95% | (h) |
| Paved Control Efficiency (vacuum sweeping twice per month) | = | 79% | (l) |
| Controlled PM-10 Paved Road Emissions | = | 0.00 | TPY |
| Controlled PM-10 Unpaved Road Emissions | = | 0.10 | TPY |

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(a) Paved Road AP-42 Emission Factor (lb/VMT) $E = (k (sL/2)^{0.65} (W/3)^{1.5} - C) * (1-(P/4/N))$

(b) Unpaved Road AP-42 Emission Factor (lb/VMT) $E = (k (s/12)^a (W/3)^b) * ((365-p)/365)$

Lime Supply

| | | | |
|--|-------|-------------------|--------|
| Average Round Trip Distance | = | 0.0 miles Paved | |
| | = | 3.9 miles Unpaved | |
| Tons per year (m) | = | 6,570.00 tons/yr | |
| tons per truck (n) | = | 20 tons/truck | |
| Trucks per year | = | 329 trucks/yr | loaded |
| Paved Constant PM-10 (lb/VMT) | k = | 0.016 (i) | |
| Paved Constant PM (lb/VMT) | k = | 0.082 (i) | |
| Paved Paved Silt Loading (g/m ²) | sL = | 9.7 (j) | |
| Paved 1980's Vehicle Fleet Emission Factor PM-10 (lb/VMT) | C = | 0.00047 (k) | |
| Paved 1980's Vehicle Fleet Emission Factor PM (lb/VMT) | C = | 0.00047 (k) | |
| Unpaved Constant PM-10 (lb/VMT) | k = | 1.5 (c) | |
| Unpaved Constant PM (lb/VMT) | k = | 4.9 (c) | |
| Unpaved Surface Material Silt Content (%) | s = | 8.4 (d) | |
| Unpaved Constant PM-10 (lb/VMT) | a = | 0.9 (c) | |
| Unpaved Constant PM (lb/VMT) | a = | 0.7 (c) | |
| Unpaved Constant PM-10 (lb/VMT) | b = | 0.45 (c) | |
| Unpaved Constant PM (lb/VMT) | b = | 0.45 (c) | |
| Average Fleet Truck weight (ton) | W = | 33 (e) | |
| Annual days with rain | p = | 73.7 (f) | |
| Number of days in precipitation averaging period | N = | 365 | |
| Paved Road Uncontrolled Emission Factor PM10 (lb/VMT) | E = | 1.5 | |
| Paved Road Uncontrolled Emission Factor PM (lb/VMT) | E = | 7.7 | |
| Unpaved Road Uncontrolled Emission Factor PM10 (lb/VMT) | E = | 2.5 | |
| Unpaved Road Uncontrolled Emission Factor PM (lb/VMT) | E = | 8.9 | |
| Paved Annual Vehicle Miles (VMT) | VMT = | 0 (g) | |
| Unpaved Annual Vehicle Miles (VMT) | VMT = | 1,282 (g) | |
| Unpaved Mg/Ci Control Efficiency and reduce speed | = | 95% (h) | |
| Paved Control Efficiency (vacuum sweeping twice per month) | = | 79% (l) | |
| Controlled PM-10 Paved Road Emissions | = | 0.00 TPY | |
| Controlled PM-10 Unpaved Road Emissions | = | 0.29 TPY | |

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(a) Paved Road AP-42 Emission Factor (lb/VMT) $E = (k (sL/2)^{0.65} (W/3)^{1.5} - C) * (1-(P/4/N))$

(b) Unpaved Road AP-42 Emission Factor (lb/VMT) $E = (k (s/12)^a (W/3)^b) * ((365-p)/365)$

Sorbent Supply

| | | | |
|--|-------|-------------------|--------|
| Average Round Trip Distance | = | 0.0 miles Paved | |
| | = | 3.9 miles Unpaved | |
| Tons per year (m) | = | 6,745.00 tons/yr | |
| tons per truck (n) | = | 20 tons/truck | |
| Trucks per year | = | 337 trucks/yr | loaded |
| Paved Constant PM-10 (lb/VMT) | k = | 0.016 (i) | |
| Paved Constant PM (lb/VMT) | k = | 0.082 (i) | |
| Paved Paved Silt Loading (g/m ²) | sL = | 9.7 (j) | |
| Paved 1980's Vehicle Fleet Emission Factor PM-10 (lb/VMT) | C = | 0.00047 (k) | |
| Paved 1980's Vehicle Fleet Emission Factor PM (lb/VMT) | C = | 0.00047 (k) | |
| Unpaved Constant PM-10 (lb/VMT) | k = | 1.5 (c) | |
| Unpaved Constant PM (lb/VMT) | k = | 4.9 (c) | |
| Unpaved Surface Material Silt Content (%) | s = | 8.4 (d) | |
| Unpaved Constant PM-10 (lb/VMT) | a = | 0.9 (c) | |
| Unpaved Constant PM (lb/VMT) | a = | 0.7 (c) | |
| Unpaved Constant PM-10 (lb/VMT) | b = | 0.45 (c) | |
| Unpaved Constant PM (lb/VMT) | b = | 0.45 (c) | |
| Average Fleet Truck weight (ton) | W = | 33 (e) | |
| Annual days with rain | p = | 73.7 (f) | |
| Number of days in precipitation averaging period | N = | 365 | |
| Paved Road Uncontrolled Emission Factor PM10 (lb/VMT) | E = | 1.5 | |
| Paved Road Uncontrolled Emission Factor PM (lb/VMT) | E = | 7.7 | |
| Unpaved Road Uncontrolled Emission Factor PM10 (lb/VMT) | E = | 2.5 | |
| Unpaved Road Uncontrolled Emission Factor PM (lb/VMT) | E = | 8.9 | |
| Paved Annual Vehicle Miles (VMT) | VMT = | 0 (g) | |
| Unpaved Annual Vehicle Miles (VMT) | VMT = | 1,316 (g) | |
| Unpaved Mg/Ci Control Efficiency and reduce speed | = | 95% (h) | |
| Paved Control Efficiency (vacuum sweeping twice per month) | = | 79% (l) | |
| Controlled PM-10 Paved Road Emissions | = | 0.00 TPY | |
| Controlled PM-10 Unpaved Road Emissions | = | 0.29 TPY | |

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(a) Paved Road AP-42 Emission Factor (lb/VMT) $E = (k (sL/2)^{0.65} (W/3)^{1.5} - C) * (1-(P/4/N))$

(b) Unpaved Road AP-42 Emission Factor (lb/VMT) $E = (k (s/12)^a (W/3)^b) * ((365-p)/365)$

Magnesium Hydroxide Supply

| | | | |
|--|-------|-------------------|---------------------------|
| Average Round Trip Distance | = | 0.0 miles Paved | |
| | = | 3.9 miles Unpaved | |
| Tons per year (m) | = | 1,752.00 tons/yr | assumed equivalent to NH3 |
| tons per truck (n) | = | 20 tons/truck | |
| Trucks per year | = | 88 trucks/yr | loaded |
| Paved Constant PM-10 (lb/VMT) | k = | 0.016 (i) | |
| Paved Constant PM (lb/VMT) | k = | 0.082 (i) | |
| Paved Paved Silt Loading (g/m^2) | sL = | 9.7 (j) | |
| Paved 1980's Vehicle Fleet Emission Factor PM-10 (lb/VMT) | C = | 0.00047 (k) | |
| Paved 1980's Vehicle Fleet Emission Factor PM (lb/VMT) | C = | 0.00047 (k) | |
| Unpaved Constant PM-10 (lb/VMT) | k = | 1.5 (c) | |
| Unpaved Constant PM (lb/VMT) | k = | 4.9 (c) | |
| Unpaved Surface Material Silt Content (%) | s = | 8.4 (d) | |
| Unpaved Constant PM-10 (lb/VMT) | a = | 0.9 (c) | |
| Unpaved Constant PM (lb/VMT) | a = | 0.7 (c) | |
| Unpaved Constant PM-10 (lb/VMT) | b = | 0.45 (c) | |
| Unpaved Constant PM (lb/VMT) | b = | 0.45 (c) | |
| Average Fleet Truck weight (ton) | W = | 33 (e) | |
| Annual days with rain | p = | 73.7 (f) | |
| Number of days in precipitation averaging period | N = | 365 | |
| Paved Road Uncontrolled Emission Factor PM10 (lb/VMT) | E = | 1.5 | |
| Paved Road Uncontrolled Emission Factor PM (lb/VMT) | E = | 7.7 | |
| Unpaved Road Uncontrolled Emission Factor PM10 (lb/VMT) | E = | 2.5 | |
| Unpaved Road Uncontrolled Emission Factor PM (lb/VMT) | E = | 8.9 | |
| Paved Annual Vehicle Miles (VMT) | VMT = | 0 (g) | |
| Unpaved Annual Vehicle Miles (VMT) | VMT = | 342 (g) | |
| Unpaved Mg/Cl Control Efficiency and reduce speed | = | 95% (h) | |
| Paved Control Efficiency (vacuum sweeping twice per month) | = | 79% (l) | |
| Controlled PM-10 Paved Road Emissions | = | 0.00 TPY | |
| Controlled PM-10 Unpaved Road Emissions | = | 0.08 TPY | |

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| | | | | |
|-----|---|---|---|---|
| (a) | Paved Road AP-42 Emission Factor (lb/VMT) | E | = | $(k (sL/2)^{0.65} (W/3)^{1.5} - C) * (1-(P/4/N))$ |
| (b) | Unpaved Road AP-42 Emission Factor (lb/VMT) | E | = | $(k (s/12)^a (W/3)^b) * ((365-p)/365)$ |

Scrubber Sludge to Landfill

| | | | | |
|---|--|-----|--------------------|-------------|
| Average Round Trip Distance | | = | 0.0 miles Paved | |
| | | = | 2.8 miles Unpaved | |
| Tons per year (m) | | = | 488,887.00 tons/yr | |
| tons per truck (n) | | = | 62 tons/truck | |
| Trucks per year | | = | 7,885 trucks/yr | loaded |
| | | | | |
| Paved | Constant PM-10 (lb/VMT) | k | = | 0.016 (i) |
| Paved | Constant PM (lb/VMT) | k | = | 0.082 (i) |
| Paved | Paved Silt Loading (g/m ²) | sL | = | 9.7 (j) |
| Paved | 1980's Vehicle Fleet Emission Factor PM-10 (lb/VMT) | C | = | 0.00047 (k) |
| Paved | 1980's Vehicle Fleet Emission Factor PM (lb/VMT) | C | = | 0.00047 (k) |
| Unpaved | Constant PM-10 (lb/VMT) | k | = | 1.5 (c) |
| Unpaved | Constant PM (lb/VMT) | k | = | 4.9 (c) |
| Unpaved | Surface Material Silt Content (%) | s | = | 8.4 (d) |
| Unpaved | Constant PM-10 (lb/VMT) | a | = | 0.9 (c) |
| Unpaved | Constant PM (lb/VMT) | a | = | 0.7 (c) |
| Unpaved | Constant PM-10 (lb/VMT) | b | = | 0.45 (c) |
| Unpaved | Constant PM (lb/VMT) | b | = | 0.45 (c) |
| | Average Fleet Truck weight (ton) | W | = | 33 (e) |
| | Annual days with rain | p | = | 73.7 (f) |
| | Number of days in precipitation averaging period | N | = | 365 |
| Paved | Road Uncontrolled Emission Factor PM10 (lb/VMT) | E | = | 1.5 |
| Paved | Road Uncontrolled Emission Factor PM (lb/VMT) | E | = | 7.7 |
| Unpaved | Road Uncontrolled Emission Factor PM10 (lb/VMT) | E | = | 2.5 |
| Unpaved | Road Uncontrolled Emission Factor PM (lb/VMT) | E | = | 8.9 |
| | | | | |
| Paved | Annual Vehicle Miles (VMT) | VMT | = | 0 (g) |
| Unpaved | Annual Vehicle Miles (VMT) | VMT | = | 22,223 (g) |
| Unpaved | Mg/Ci Control Efficiency and reduce speed | | = | 95% (h) |
| Paved | Control Efficiency (vacuum sweeping twice per month) | | = | 79% (l) |
| | | | | |
| Controlled PM-10 Paved Road Emissions | | = | 0.00 | TPY |
| Controlled PM-10 Unpaved Road Emissions | | = | 1.41 | TPY |

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| | | | |
|-----|---|---|---|
| (a) | Paved Road AP-42 Emission Factor (lb/VMT) | E | $= (k (sL/2)^{0.65} (W/3)^{1.5} - C) * (1-(P/4/N))$ |
| (b) | Unpaved Road AP-42 Emission Factor (lb/VMT) | E | $= (k (s/12)^a (W/3)^b) * ((365-p)/365)$ |

Fly Ash trucked to landfill

| | | | | |
|---|--|-----|--------------------|-------------|
| Average Round Trip Distance | | = | 0.0 miles Paved | |
| | | = | 2.7 miles Unpaved | |
| Tons per year (m) | | = | 987,094.00 tons/yr | |
| tons per truck (n) | | = | 62 tons/truck | |
| Trucks per year | | = | 15,921 trucks/yr | loaded |
| | | | | |
| Paved | Constant PM-10 (lb/VMT) | k | = | 0.016 (i) |
| Paved | Constant PM (lb/VMT) | k | = | 0.082 (i) |
| Paved | Paved Silt Loading (g/m ²) | sL | = | 9.7 (j) |
| Paved | 1980's Vehicle Fleet Emission Factor PM-10 (lb/VMT) | C | = | 0.00047 (k) |
| Paved | 1980's Vehicle Fleet Emission Factor PM (lb/VMT) | C | = | 0.00047 (k) |
| Unpaved | Constant PM-10 (lb/VMT) | k | = | 1.5 (c) |
| Unpaved | Constant PM (lb/VMT) | k | = | 4.9 (c) |
| Unpaved | Surface Material Silt Content (%) | s | = | 8.4 (d) |
| Unpaved | Constant PM-10 (lb/VMT) | a | = | 0.9 (c) |
| Unpaved | Constant PM (lb/VMT) | a | = | 0.7 (c) |
| Unpaved | Constant PM-10 (lb/VMT) | b | = | 0.45 (c) |
| Unpaved | Constant PM (lb/VMT) | b | = | 0.45 (c) |
| | Average Fleet Truck weight (ton) | W | = | 33 (e) |
| | Annual days with rain | p | = | 73.7 (f) |
| | Number of days in precipitation averaging period | N | = | 365 |
| Paved | Road Uncontrolled Emission Factor PM10 (lb/VMT) | E | = | 1.5 |
| Paved | Road Uncontrolled Emission Factor PM (lb/VMT) | E | = | 7.7 |
| Unpaved | Road Uncontrolled Emission Factor PM10 (lb/VMT) | E | = | 2.5 |
| Unpaved | Road Uncontrolled Emission Factor PM (lb/VMT) | E | = | 8.9 |
| | | | | |
| Paved | Annual Vehicle Miles (VMT) | VMT | = | 0 (g) |
| Unpaved | Annual Vehicle Miles (VMT) | VMT | = | 43,663 (g) |
| Unpaved | Mg/CI Control Efficiency and reduce speed | | = | 95% (h) |
| Paved | Control Efficiency (vacuum sweeping twice per month) | | = | 79% (l) |
| | | | | |
| Controlled PM-10 Paved Road Emissions | | = | 0.00 | TPY |
| Controlled PM-10 Unpaved Road Emissions | | = | 2.77 | TPY |

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| | | | |
|-----|---|---|---|
| (a) | Paved Road AP-42 Emission Factor (lb/VMT) | E | $= (k (sL/2)^{0.65} (W/3)^{1.5} - C) * (1-(P/4/N))$ |
| (b) | Unpaved Road AP-42 Emission Factor (lb/VMT) | E | $= (k (s/12)^a (W/3)^b) * ((365-p)/365)$ |

Bottom Ash trucked to landfill

| | | | | |
|---|--|-----|--------------------|-------------|
| Average Round Trip Distance | | = | 0.0 miles Paved | |
| | | = | 3.1 miles Unpaved | |
| Tons per year (m) | | = | 246,769.00 tons/yr | |
| tons per truck (n) | | = | 62 tons/truck | |
| Trucks per year | | = | 3,980 trucks/yr | loaded |
| | | | | |
| Paved | Constant PM-10 (lb/VMT) | k | = | 0.016 (i) |
| Paved | Constant PM (lb/VMT) | k | = | 0.082 (i) |
| Paved | Paved Silt Loading (g/m ²) | sL | = | 9.7 (j) |
| Paved | 1980's Vehicle Fleet Emission Factor PM-10 (lb/VMT) | C | = | 0.00047 (k) |
| Paved | 1980's Vehicle Fleet Emission Factor PM (lb/VMT) | C | = | 0.00047 (k) |
| Unpaved | Constant PM-10 (lb/VMT) | k | = | 1.5 (c) |
| Unpaved | Constant PM (lb/VMT) | k | = | 4.9 (c) |
| Unpaved | Surface Material Silt Content (%) | s | = | 8.4 (d) |
| Unpaved | Constant PM-10 (lb/VMT) | a | = | 0.9 (c) |
| Unpaved | Constant PM (lb/VMT) | a | = | 0.7 (c) |
| Unpaved | Constant PM-10 (lb/VMT) | b | = | 0.45 (c) |
| Unpaved | Constant PM (lb/VMT) | b | = | 0.45 (c) |
| | Average Fleet Truck weight (ton) | W | = | 33 (e) |
| | Annual days with rain | p | = | 73.7 (f) |
| | Number of days in precipitation averaging period | N | = | 365 |
| Paved | Road Uncontrolled Emission Factor PM10 (lb/VMT) | E | = | 1.5 |
| Paved | Road Uncontrolled Emission Factor PM (lb/VMT) | E | = | 7.7 |
| Unpaved | Road Uncontrolled Emission Factor PM10 (lb/VMT) | E | = | 2.5 |
| Unpaved | Road Uncontrolled Emission Factor PM (lb/VMT) | E | = | 8.9 |
| | | | | |
| Paved | Annual Vehicle Miles (VMT) | VMT | = | 0 (g) |
| Unpaved | Annual Vehicle Miles (VMT) | VMT | = | 12,423 (g) |
| Unpaved | Mg/CI Control Efficiency and reduce speed | | = | 95% (h) |
| Paved | Control Efficiency (vacuum sweeping twice per month) | | = | 79% (l) |
| | | | | |
| Controlled PM-10 Paved Road Emissions | | = | 0.00 | TPY |
| Controlled PM-10 Unpaved Road Emissions | | = | 0.79 | TPY |

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| | | | |
|-----|---|---|---|
| (a) | Paved Road AP-42 Emission Factor (lb/VMT) | E | = $(k (sL/2)^{0.65} (W/3)^{1.5} - C) * (1-(P/4/N))$ |
| (b) | Unpaved Road AP-42 Emission Factor (lb/VMT) | E | = $(k (s/12)^a (W/3)^b) * ((365-p)/365)$ |

Notes:

- (a) AP-42 Section 13.2.1, Equation 2; December 2003
- (b) AP-42 Section 13.2.2, Equation 2; December 2003
- (c) AP-42, Section 13.2.2, Table 13.2.2-2 for industrial roads (Dec. 2003)
- (d) AP-42, Section 13.2.2, Table 13.2.2-1, Western Surface Coal Mining-haul road to/from pit (Dec. 2003)
- (e) Average of loaded and unloaded truck weights estimated by Burns & McDonnell
- (f) Average number of days reporting 0.01" or more of precipitation per year in Ely, Nevada. Climate Normals Data based on 1961 - 1990 record period.
- (g) VMT are calculated from estimated tons per year trucked
- (h) AP-42 Section 13.2.2.3, "Past field testing of emissions from controlled unpaved roads has shown that chemical dust suppressants provide a PM10 control efficiency of about 80 percent when applied at regular intervals of 2 weeks to 1 month."
- (i) AP-42, Section 13.2.1, Table 13.2-1.1 (Dec. 2003)
- (j) AP-42, Section 13.2.1, Table 13.2.1-4 for Iron & Steel Production (Dec. 2003)
- (k) AP-42, Section 13.2.1, Table 13.2.1-2 (Dec. 2003)
- (l) Air Pollution Training Institute (APTI) course 4.19b "Preparation of Fine Particulate Emission Inventories" Chapter 7: Fugitive Dust Area Sources
- (m) Estimated by C&B
- (n) Estimated by C&B

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ROAD HAUL LENGTH CALCULATIONS

| Road ID | Length (ft) | Length (m) | Thickness (m) | Adjusted width (m) | Max Number of volume sources - N | volume sources modeled | Volume source spacing (m) | source height ^a (m) | sigma (y0) | sigma (z0) | Release Height (m) |
|--------------------------|----------------|---------------|------------------|--------------------------|--|------------------------------|---------------------------------|--------------------------------------|------------|------------|-----------------------|
| Material Supply by truck | | | | | | | | | | | |
| H8 - H6 | 7200 | 2194.56 | 6.5 | 12.5 | 176 | 88 | 25 | 9.144 | 11.63 | 4.25 | 4.57 |
| H6 - H3 | 1100 | 335.28 | 6.5 | 12.5 | 27 | 13 | 25 | 9.144 | 11.63 | 4.25 | 4.57 |
| H3 - H4 | 100 | 30.48 | 6.5 | 12.5 | 2 | 2 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| H4 - G2 | 200 | 60.96 | 6.5 | 12.5 | 5 | 5 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| G2 - F1 | 200 | 60.96 | 6.5 | 12.5 | 5 | 5 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| F1 - E3 | 200 | 60.96 | 6.5 | 12.5 | 5 | 5 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| E3 - E1 | 300 | 91.44 | 6.5 | 12.5 | 7 | 7 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| E1 - D3 | 200 | 60.96 | 6.5 | 12.5 | 5 | 5 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| D3 - D4 | 300 | 91.44 | 6.5 | 12.5 | 7 | 7 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| D4 - D5 | 300 | 91.44 | 6.5 | 12.5 | 7 | 7 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| D5 - D8 | 200 | 60.96 | 6.5 | 12.5 | 5 | 5 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| total miles | | 1.95 | | | | | | | | | |
| Bottom Ash to Landfill | | | | | | | | | | | |
| F2 - F1 | 500 | 152.4 | 6.5 | 12.5 | 12 | 6 | 25 | 9.144 | 11.63 | 4.25 | 4.57 |
| F1 - E3 | 200 | 60.96 | 6.5 | 12.5 | 5 | 5 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| E3 - E1 | 400 | 121.92 | 6.5 | 12.5 | 10 | 10 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| E1 - D3 | 200 | 60.96 | 6.5 | 12.5 | 5 | 5 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| D3 - D1 | 400 | 121.92 | 6.5 | 12.5 | 10 | 10 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| D1 - C2 | 100 | 30.48 | 6.5 | 12.5 | 2 | 2 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| C2 - C3 | 600 | 182.88 | 6.5 | 12.5 | 15 | 7 | 25 | 9.144 | 11.63 | 4.25 | 4.57 |
| C3 - C4 | 900 | 274.32 | 6.5 | 12.5 | 22 | 11 | 25 | 9.144 | 11.63 | 4.25 | 4.57 |
| LF | | 1505.3 | 6.5 | 12.5 | 120 | 60 | 25 | 9.144 | 11.63 | 4.25 | 4.57 |
| total miles | | 1.56 | | | | | | | | | |
| Fly Ash to Landfill | | | | | | | | | | | |
| D2 - D1 | 700 | 213.36 | 6.5 | 12.5 | 17 | 17 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| D1 - C2 | 100 | 30.48 | 6.5 | 12.5 | 2 | 2 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| C2 - C3 | 600 | 182.88 | 6.5 | 12.5 | 15 | 7 | 25 | 9.144 | 11.63 | 4.25 | 4.57 |
| C3 - C4 | 900 | 274.32 | 6.5 | 12.5 | 22 | 11 | 25 | 9.144 | 11.63 | 4.25 | 4.57 |
| LF | | 1505.3 | 6.5 | 12.5 | 120 | 60 | 25 | 9.144 | 11.63 | 4.25 | 4.57 |
| total miles | | 1.37 | | | | | | | | | |

A6-54
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
ROAD HAUL LENGTH CALCULATIONS

| Road ID | Length (ft) | Length (m) | Thickness (m) | Adjusted width (m) | Max Number of volume sources - N | volume sources modeled | Volume source spacing (m) | source height ^a (m) | sigma (y0) | sigma (z0) | Release Height (m) |
|------------------------------------|----------------|---------------|------------------|--------------------------|--|------------------------------|---------------------------------|--------------------------------------|------------|------------|-----------------------|
| Scrubber Sludge to Landfill | | | | | | | | | | | |
| D7 - D4 | 200 | 60.96 | 6.5 | 12.5 | 5 | 5 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| D4 - D3 | 300 | 91.44 | 6.5 | 12.5 | 7 | 7 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| D3 - D1 | 400 | 121.92 | 6.5 | 12.5 | 10 | 10 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| D1 - C2 | 100 | 30.48 | 6.5 | 12.5 | 2 | 2 | 13 | 9.144 | 5.81 | 4.25 | 4.57 |
| C2 - C3 | 600 | 182.88 | 6.5 | 12.5 | 15 | 7 | 25 | 9.144 | 11.63 | 4.25 | 4.57 |
| C3 - C4 | 900 | 274.32 | 6.5 | 12.5 | 22 | 11 | 25 | 9.144 | 11.63 | 4.25 | 4.57 |
| LF | | 1505.3 | 6.5 | 12.5 | 120 | 60 | 25 | 9.144 | 11.63 | 4.25 | 4.57 |
| total miles | | 1.41 | | | | | | | | | |

Notes:

a Truck height assumed to be 15 ft.

Suggested Steps when modeling using the Texas Protocol:

- 1) Determine the adjusted width of the road. The adjusted width is the actual width plus 6 meters. The additional width represents turbulence caused by the vehicle as it moves along the road.
- 2) Determine the number of volume sources, N. Divide the length of the road by the adjusted width. The result is the maximum number of volume sources that could be used to represent the road.
- 3) Determine the height of the volume. The height is equal to twice the height of the vehicle generating the emissions.
- 4) Determine the initial horizontal sigma for each volume:
 - a) If the road is represented by a single volume, divide the adjusted width by 4.3.
 - b) If the road is represented by adjacent volumes, divide the adjusted width by 2.15.
 - c) If the road is represented by alternating volumes, divide twice the adjusted width - measured from the center point of the first volume to the center point of the next volume - by 2.15.
- 5) Determine the initial vertical sigma. Divide the height of the volume determined in Step 3 by 2.15.
- 6) Determine the release point. Divide the height of the volume by two. This point is the center of the volume.
- 7) Determine the emission rate for each volume used to calculate the initial horizontal sigma in Step 4. Divide the total emission rate equally among the individual volumes used to represent the road.
- 8) Determine the UTM coordinate for the release point. The release point location is in the center of the base of the volume. This location must be at least one meter from the nearest receptor.

A6-55
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
ROAD HAUL APPORTIONMENT CALCULATIONS

| Emissions by Road Segment | | | | | | | | | | | average hours of operation | | 8760 | 4380 | | |
|---------------------------|----------|--------|--|---------|--|-----------------------------|----------------------------|------------------------|------------------------|--|---|----------------------------------|-------------------------------------|---|--|-------------------------------|
| Haul Road | Source | X | | Y | | Emissions (tpy) | | | | | | | | Annual Average Emission Rate (g/s) | Maximum Assumed Short Term Emission Rate ¹ (g/s) | |
| | | | | | | Limestone Haul Trucks | Soda Ash Haul Trucks | Lime Haul Trucks | Sorbent Haul Trucks | Magnesium Hydroxide Haul Trucks | Scrubber Sludge Hauled to Landfill | Fly Ash Hauled to Landfill | Bottom Ash Hauled to Landfill | | | Total Hauling (All Routes) |
| H8 - H6 | H8_H6_1 | 691971 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_2 | 691946 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_3 | 691921 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_4 | 691896 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_5 | 691871 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_6 | 691846 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_7 | 691821 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_8 | 691796 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_9 | 691771 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_10 | 691746 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_11 | 691721 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_12 | 691696 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_13 | 691671 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_14 | 691646 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_15 | 691621 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_16 | 691596 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_17 | 691571 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_18 | 691546 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_19 | 691521 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_20 | 691496 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_21 | 691471 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_22 | 691446 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_23 | 691421 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_24 | 691396 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_25 | 691371 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_26 | 691346 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_27 | 691321 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_28 | 691296 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_29 | 691271 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_30 | 691246 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_31 | 691221 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_32 | 691196 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_33 | 691171 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_34 | 691146 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_35 | 691121 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_36 | 691096 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_37 | 691071 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_38 | 691046 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_39 | 691021 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_40 | 690996 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_41 | 690971 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_42 | 690946 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_43 | 690921 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_44 | 690896 | | 4374082 | | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |

A6-55
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
ROAD HAUL APPORTIONMENT CALCULATIONS

| Emissions by Road Segment | | | | | | | | | | | | average hours of operation | 8760 | 4380 |
|---------------------------|----------|--------------------------|---------|-----------------------|----------------------|------------------|---------------------|---------------------------------|------------------------------------|----------------------------|-------------------------------|----------------------------|------------------------------------|---|
| Haul Road | Source | X Y | | Emissions (tpy) | | | | | | | | | Annual Average Emission Rate (g/s) | Maximum Assumed Short Term Emission Rate ¹ (g/s) |
| | | | | Limestone Haul Trucks | Soda Ash Haul Trucks | Lime Haul Trucks | Sorbent Haul Trucks | Magnesium Hydroxide Haul Trucks | Scrubber Sludge Hauled to Landfill | Fly Ash Hauled to Landfill | Bottom Ash Hauled to Landfill | Total Hauling (All Routes) | | |
| H8 - H6 (Continued) | H8_H6_45 | 690871 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_46 | 690846 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_47 | 690821 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_48 | 690796 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_49 | 690771 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_50 | 690746 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_51 | 690721 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_52 | 690696 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_53 | 690671 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_54 | 690646 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_55 | 690621 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_56 | 690596 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_57 | 690571 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_58 | 690546 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_59 | 690521 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_60 | 690496 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_61 | 690471 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_62 | 690446 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_63 | 690421 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_64 | 690396 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_65 | 690371 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_66 | 690346 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_67 | 690321 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_68 | 690296 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_69 | 690271 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_70 | 690246 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_71 | 690221 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_72 | 690196 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_73 | 690171 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_74 | 690146 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_75 | 690121 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_76 | 690096 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_77 | 690071 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_78 | 690071 | 4374082 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_79 | 690046 | 4374084 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_80 | 690022 | 4374090 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_81 | 689999 | 4374100 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_82 | 689977 | 4374113 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_83 | 689959 | 4374129 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_84 | 689943 | 4374149 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_85 | 689930 | 4374170 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_86 | 689921 | 4374194 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_87 | 689916 | 4374218 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H8_H6_88 | 689915 | 4374243 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |

A6-55
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
ROAD HAUL APPORTIONMENT CALCULATIONS

| Emissions by Road Segment | | | | | | | | | | | | average hours of operation | 8760 | 4380 |
|---------------------------|----------|--------------------------|---------|-----------------------|----------------------|------------------|---------------------|---------------------------------|------------------------------------|----------------------------|-------------------------------|----------------------------|------------------------------------|---|
| Haul Road | Source | X Y | | Emissions (tpy) | | | | | | | | | Annual Average Emission Rate (g/s) | Maximum Assumed Short Term Emission Rate ¹ (g/s) |
| | | | | Limestone Haul Trucks | Soda Ash Haul Trucks | Lime Haul Trucks | Sorbent Haul Trucks | Magnesium Hydroxide Haul Trucks | Scrubber Sludge Hauled to Landfill | Fly Ash Hauled to Landfill | Bottom Ash Hauled to Landfill | Total Hauling (All Routes) | | |
| H6 - H3 | H6_H3_1 | 689915 | 4374268 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H6_H3_2 | 689915 | 4374293 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H6_H3_3 | 689915 | 4374318 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H6_H3_4 | 689915 | 4374343 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H6_H3_5 | 689915 | 4374368 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H6_H3_6 | 689915 | 4374393 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H6_H3_7 | 689915 | 4374418 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H6_H3_8 | 689915 | 4374443 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H6_H3_9 | 689915 | 4374468 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H6_H3_10 | 689915 | 4374493 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H6_H3_11 | 689915 | 4374518 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| H3 - H4 | H3_H4_1 | 689915 | 4374535 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H3_H4_2 | 689928 | 4374535 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H3_H4_3 | 689941 | 4374535 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H3_H4_4 | 689954 | 4374535 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| H4 - G2 | H4_G2_1 | 689957 | 4374535 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H4_G2_2 | 689957 | 4374548 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H4_G2_3 | 689957 | 4374561 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H4_G2_4 | 689957 | 4374574 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | H4_G2_5 | 689957 | 4374587 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| G2 - F1 | G2_F1_1 | 689957 | 4374592 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | G2_F1_2 | 689957 | 4374605 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | G2_F1_3 | 689957 | 4374618 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | G2_F1_4 | 689957 | 4374631 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | G2_F1_5 | 689957 | 4374644 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | G2_F1_6 | 689957 | 4374657 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | G2_F1_7 | 689957 | 4374670 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | G2_F1_8 | 689957 | 4374683 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| F1 - E3 | F1_E3_1 | 689957 | 4374694 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| | F1_E3_2 | 689957 | 4374707 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| | F1_E3_3 | 689957 | 4374720 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| | F1_E3_4 | 689957 | 4374733 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| | F1_E3_5 | 689957 | 4374746 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| E3 - E1 | E3_E1_1 | 689957 | 4374748 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| | E3_E1_2 | 689957 | 4374765 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| | E3_E1_3 | 689957 | 4374778 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| | E3_E1_4 | 689957 | 4374791 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| | E3_E1_5 | 689957 | 4374804 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| | E3_E1_6 | 689957 | 4374817 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| | E3_E1_7 | 689957 | 4374830 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| | E3_E1_8 | 689957 | 4374843 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |

A6-55
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
ROAD HAUL APPORTIONMENT CALCULATIONS

| Emissions by Road Segment | | | | | | | | | | | | average hours of operation | 8760 | 4380 |
|---------------------------|---------|--------------------------|---------|-----------------------|----------------------|------------------|---------------------|---------------------------------|------------------------------------|----------------------------|-------------------------------|----------------------------|------------------------------------|---|
| Haul Road | Source | X Y | | Emissions (tpy) | | | | | | | | | Annual Average Emission Rate (g/s) | Maximum Assumed Short Term Emission Rate ¹ (g/s) |
| | | | | Limestone Haul Trucks | Soda Ash Haul Trucks | Lime Haul Trucks | Sorbent Haul Trucks | Magnesium Hydroxide Haul Trucks | Scrubber Sludge Hauled to Landfill | Fly Ash Hauled to Landfill | Bottom Ash Hauled to Landfill | Total Hauling (All Routes) | | |
| E1 - D3 | E1_D3_1 | 689957 | 4374853 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| | E1_D3_2 | 689957 | 4374866 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| | E1_D3_3 | 689957 | 4374879 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| | E1_D3_4 | 689957 | 4374892 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| | E1_D3_5 | 689959 | 4374905 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| | E1_D3_6 | 689966 | 4374916 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | 0.023 | | 0.03 | 0.00090 | 0.00180 |
| D3 - D4 | D3_D4_1 | 689967 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | 0.013 | | | 0.02 | 0.00060 | 0.00120 |
| | D3_D4_2 | 689979 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | 0.013 | | | 0.02 | 0.00060 | 0.00120 |
| | D3_D4_3 | 689992 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | 0.013 | | | 0.02 | 0.00060 | 0.00120 |
| | D3_D4_4 | 690005 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | 0.013 | | | 0.02 | 0.00060 | 0.00120 |
| | D3_D4_5 | 690018 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | 0.013 | | | 0.02 | 0.00060 | 0.00120 |
| | D3_D4_6 | 690031 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | 0.013 | | | 0.02 | 0.00060 | 0.00120 |
| | D3_D4_7 | 690044 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | 0.013 | | | 0.02 | 0.00060 | 0.00120 |
| | D3_D4_8 | 690057 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | 0.013 | | | 0.02 | 0.00060 | 0.00120 |
| D4 - D5 | D4_D5_1 | 690062 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | D4_D5_2 | 690075 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | D4_D5_3 | 690088 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | D4_D5_4 | 690101 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | D4_D5_5 | 690114 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | D4_D5_6 | 690127 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | D4_D5_7 | 690140 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | D4_D5_8 | 690153 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| D5 - D8 | D5_D8_1 | 690154 | 4374918 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | D5_D8_2 | 690154 | 4374905 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | D5_D8_3 | 690154 | 4374892 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | D5_D8_4 | 690154 | 4374879 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | D5_D8_5 | 690154 | 4374866 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | D5_D8_6 | 690154 | 4374853 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| | D5_D8_7 | 690154 | 4374842 | 0.003 | 0.001 | 0.002 | 0.002 | 0.000 | | | | 0.01 | 0.00023 | 0.00045 |
| D7 - D4 | D7_D4_1 | 690062 | 4374842 | | | | | | 0.013 | | | 0.01 | 0.00038 | 0.00075 |
| | D7_D4_2 | 690062 | 4374853 | | | | | | 0.013 | | | 0.01 | 0.00038 | 0.00075 |
| | D7_D4_3 | 690062 | 4374866 | | | | | | 0.013 | | | 0.01 | 0.00038 | 0.00075 |
| | D7_D4_4 | 690062 | 4374879 | | | | | | 0.013 | | | 0.01 | 0.00038 | 0.00075 |
| | D7_D4_5 | 690062 | 4374892 | | | | | | 0.013 | | | 0.01 | 0.00038 | 0.00075 |
| | D7_D4_6 | 690062 | 4374905 | | | | | | 0.013 | | | 0.01 | 0.00038 | 0.00075 |
| | D7_D4_7 | 690062 | 4374918 | | | | | | 0.013 | | | 0.01 | 0.00038 | 0.00075 |
| F2 - F1 | F2_F1_1 | 690104 | 4374694 | | | | | | | 0.023 | | 0.02 | 0.00068 | 0.00135 |
| | F2_F1_2 | 690079 | 4374694 | | | | | | | 0.023 | | 0.02 | 0.00068 | 0.00135 |
| | F2_F1_3 | 690054 | 4374694 | | | | | | | 0.023 | | 0.02 | 0.00068 | 0.00135 |
| | F2_F1_4 | 690029 | 4374694 | | | | | | | 0.023 | | 0.02 | 0.00068 | 0.00135 |
| | F2_F1_5 | 690004 | 4374694 | | | | | | | 0.023 | | 0.02 | 0.00068 | 0.00135 |
| | F2_F1_6 | 689979 | 4374694 | | | | | | | 0.023 | | 0.02 | 0.00068 | 0.00135 |

A6-55
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
ROAD HAUL APPORTIONMENT CALCULATIONS

| Emissions by Road Segment | | | | | | | | | | average hours of operation | | 8760 | 4380 | | |
|---------------------------|----------|--------|---------|---|--|-----------------------------|----------------------------|------------------------|------------------------|--|---|----------------------------------|-------------------------------------|---|--|
| Haul Road | Source | X | | Y | | Emissions (tpy) | | | | | | | | Annual Average Emission Rate (g/s) | Maximum Assumed Short Term Emission Rate ¹ (g/s) |
| | | | | | | Limestone Haul Trucks | Soda Ash Haul Trucks | Lime Haul Trucks | Sorbent Haul Trucks | Magnesium Hydroxide Haul Trucks | Scrubber Sludge Hauled to Landfill | Fly Ash Hauled to Landfill | Bottom Ash Hauled to Landfill | | |
| D3 - D1 | D3_D1_1 | 689967 | 4374918 | | | | | | 0.013 | 0.023 | | 0.04 | 0.00105 | 0.00210 | |
| | D3_D1_2 | 689975 | 4374926 | | | | | | 0.013 | 0.023 | | 0.04 | 0.00105 | 0.00210 | |
| | D3_D1_3 | 689984 | 4374936 | | | | | | 0.013 | 0.023 | | 0.04 | 0.00105 | 0.00210 | |
| | D3_D1_4 | 689993 | 4374945 | | | | | | 0.013 | 0.023 | | 0.04 | 0.00105 | 0.00210 | |
| | D3_D1_5 | 690003 | 4374954 | | | | | | 0.013 | 0.023 | | 0.04 | 0.00105 | 0.00210 | |
| | D3_D1_6 | 690012 | 4374963 | | | | | | 0.013 | 0.023 | | 0.04 | 0.00105 | 0.00210 | |
| | D3_D1_7 | 690021 | 4374972 | | | | | | 0.013 | 0.023 | | 0.04 | 0.00105 | 0.00210 | |
| | D3_D1_8 | 690030 | 4374981 | | | | | | 0.013 | 0.023 | | 0.04 | 0.00105 | 0.00210 | |
| | D3_D1_9 | 690039 | 4374991 | | | | | | 0.013 | 0.023 | | 0.04 | 0.00105 | 0.00210 | |
| D2 - D1 | D2_D1_1 | 690061 | 4374999 | | | | | | | | 0.008 | 0.01 | 0.00023 | 0.00045 | |
| | D2_D1_2 | 690074 | 4374999 | | | | | | | | 0.008 | 0.01 | 0.00023 | 0.00045 | |
| | D2_D1_3 | 690087 | 4374999 | | | | | | | | 0.008 | 0.01 | 0.00023 | 0.00045 | |
| | D2_D1_4 | 690100 | 4374999 | | | | | | | | 0.008 | 0.01 | 0.00023 | 0.00045 | |
| | D2_D1_5 | 690113 | 4374999 | | | | | | | | 0.008 | 0.01 | 0.00023 | 0.00045 | |
| | D2_D1_6 | 690126 | 4374999 | | | | | | | | 0.008 | 0.01 | 0.00023 | 0.00045 | |
| | D2_D1_7 | 690139 | 4374999 | | | | | | | | 0.008 | 0.01 | 0.00023 | 0.00045 | |
| | D2_D1_8 | 690152 | 4374999 | | | | | | | | 0.008 | 0.01 | 0.00023 | 0.00045 | |
| | D2_D1_9 | 690165 | 4374999 | | | | | | | | 0.008 | 0.01 | 0.00023 | 0.00045 | |
| | D2_D1_10 | 690178 | 4374999 | | | | | | | | 0.008 | 0.01 | 0.00023 | 0.00045 | |
| | D2_D1_11 | 690191 | 4374999 | | | | | | | | 0.008 | 0.01 | 0.00023 | 0.00045 | |
| | D2_D1_12 | 690204 | 4374999 | | | | | | | | 0.008 | 0.01 | 0.00023 | 0.00045 | |
| | D2_D1_13 | 690217 | 4374999 | | | | | | | | 0.008 | 0.01 | 0.00023 | 0.00045 | |
| | D2_D1_14 | 690230 | 4374999 | | | | | | | | 0.008 | 0.01 | 0.00023 | 0.00045 | |
| | D2_D1_15 | 690243 | 4374999 | | | | | | | | 0.008 | 0.01 | 0.00023 | 0.00045 | |
| | D2_D1_16 | 690248 | 4374999 | | | | | | | | 0.008 | 0.01 | 0.00023 | 0.00045 | |
| D1 - C2 | D1_C2_1 | 690048 | 4374999 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | D1_C2_2 | 690048 | 4375012 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | D1_C2_3 | 690048 | 4375025 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | D1_C2_4 | 690048 | 4375038 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | D1_C2_5 | 690048 | 4375051 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| C2 - C3 | C2_C3_1 | 690048 | 4375057 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C2_C3_2 | 690073 | 4375057 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C2_C3_3 | 690098 | 4375057 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C2_C3_4 | 690123 | 4375057 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C2_C3_5 | 690148 | 4375057 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C2_C3_6 | 690173 | 4375057 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C2_C3_7 | 690198 | 4375057 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C2_C3_8 | 690223 | 4375057 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C2_C3_9 | 690248 | 4375057 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |

A6-55
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
ROAD HAUL APPORTIONMENT CALCULATIONS

| Emissions by Road Segment | | | | | | | | | | | average hours of operation | | 8760 | 4380 | |
|---------------------------|----------|--------|---------|---|--|-----------------------------|----------------------------|------------------------|------------------------|--|---|----------------------------------|-------------------------------------|---|--|
| Haul Road | Source | X | | Y | | Emissions (tpy) | | | | | | | | Annual Average Emission Rate (g/s) | Maximum Assumed Short Term Emission Rate ¹ (g/s) |
| | | | | | | Limestone Haul Trucks | Soda Ash Haul Trucks | Lime Haul Trucks | Sorbent Haul Trucks | Magnesium Hydroxide Haul Trucks | Scrubber Sludge Hauled to Landfill | Fly Ash Hauled to Landfill | Bottom Ash Hauled to Landfill | | |
| C3 - C4 | C3_C4_1 | 690248 | 4375057 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C3_C4_2 | 690248 | 4375082 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C3_C4_3 | 690248 | 4375107 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C3_C4_4 | 690248 | 4375132 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C3_C4_5 | 690249 | 4375157 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C3_C4_6 | 690251 | 4375182 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C3_C4_7 | 690256 | 4375207 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C3_C4_8 | 690262 | 4375231 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C3_C4_9 | 690268 | 4375255 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | C3_C4_10 | 690274 | 4375279 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| Landfill | LF_1 | 690281 | 4375305 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_2 | 690293 | 4375327 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_3 | 690310 | 4375345 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_4 | 690329 | 4375361 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_5 | 690345 | 4375379 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_6 | 690358 | 4375401 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_7 | 690365 | 4375424 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_8 | 690367 | 4375449 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_9 | 690368 | 4375474 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_10 | 690368 | 4375499 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_11 | 690368 | 4375524 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_12 | 690368 | 4375549 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_13 | 690368 | 4375574 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_14 | 690369 | 4375599 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_15 | 690369 | 4375624 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_16 | 690369 | 4375649 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_17 | 690369 | 4375674 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_18 | 690369 | 4375699 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_19 | 690369 | 4375724 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_20 | 690366 | 4375749 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_21 | 690362 | 4375774 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_22 | 690357 | 4375798 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_23 | 690350 | 4375822 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_24 | 690343 | 4375846 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_25 | 690334 | 4375869 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_26 | 690322 | 4375891 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_27 | 690311 | 4375913 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_28 | 690298 | 4375935 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_29 | 690284 | 4375956 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_30 | 690270 | 4375976 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_31 | 690254 | 4375995 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_32 | 690236 | 4376013 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_33 | 690219 | 4376031 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |
| | LF_34 | 690199 | 4376047 | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 | |

A6-55
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
ROAD HAUL APPORTIONMENT CALCULATIONS

| Emissions by Road Segment | | | | | | | | | | | average hours of operation | | 8760 | 4380 | |
|---------------------------|--------|--------|---------|---|--|-----------------------------|----------------------------|------------------------|------------------------|--|---|----------------------------------|-------------------------------------|---|--|
| Haul Road | Source | X | | Y | | Emissions (tpy) | | | | | | | | Annual Average Emission Rate (g/s) | Maximum Assumed Short Term Emission Rate ¹ (g/s) |
| | | | | | | Limestone Haul Trucks | Soda Ash Haul Trucks | Lime Haul Trucks | Sorbent Haul Trucks | Magnesium Hydroxide Haul Trucks | Scrubber Sludge Hauled to Landfill | Fly Ash Hauled to Landfill | Bottom Ash Hauled to Landfill | | |
| Landfill (Continued) | LF_35 | 690179 | 4376062 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_36 | 690159 | 4376077 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_37 | 690138 | 4376090 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_38 | 690117 | 4376103 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_39 | 690094 | 4376114 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_40 | 690070 | 4376120 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_41 | 690046 | 4376127 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_42 | 690022 | 4376134 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_43 | 689998 | 4376141 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_44 | 689974 | 4376147 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_45 | 689949 | 4376149 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_46 | 689924 | 4376149 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_47 | 689899 | 4376149 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_48 | 689874 | 4376149 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_49 | 689849 | 4376149 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_50 | 689824 | 4376149 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_51 | 689799 | 4376149 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_52 | 689774 | 4376149 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_53 | 689749 | 4376149 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_54 | 689724 | 4376149 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_55 | 689699 | 4376149 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_56 | 689674 | 4376149 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_57 | 689649 | 4376149 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_58 | 689624 | 4376149 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_59 | 689599 | 4376149 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |
| | LF_60 | 689574 | 4376149 | | | | | | | 0.013 | 0.023 | 0.008 | 0.04 | 0.00128 | 0.00255 |

1 - Maximum short term emissions were estimated as twice the annual averaged emission rate. This was accomplished by assuming maximum daily emissions occurred over a 12 hour period, as opposed to a 24 hour period.

A6-56
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: FE-1
Emission Source: Secondary Fuel/Startup and Emergency Power - 2,000,000 gallon diesel tank
Pollutants: VOC

see pdf

A6-57
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: FE-2
Emission Source: Rail Power Refueling - 1,000,000 gallon diesel tank
Pollutants: VOC

see pdf

A6-58
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: FE-3
Emission Source: Burner Supply - 60,000 gallon diesel tank
Pollutants: VOC

see pdf

A6-59
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: FE-4
Emission Source: Burner Supply - 60,000 gallon diesel tank
Pollutants: VOC

see pdf

A6-60
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: FE-5
Emission Source: Auxiliary Boiler/Emergency Generator - 15,000 gallon diesel tank
Pollutants: VOC

see pdf

A6-6 1
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: FE-6
Emission Source: Main Fire Water Pump - 700 gallon diesel tank
Pollutants: VOC

see pdf

A6-62
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: FE-7
Emission Source: Booster Fire Water Pump - 200 gallon diesel tank
Pollutants: VOC

see pdf

A6-63
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: FE-8
Emission Source: Emergency Quench Water Pump - 700 gallon diesel tank
Pollutants: VOC

see pdf

A6-64
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: FE-9
Emission Source: Switchyard Backup Power Supply - 700 gallon diesel tank
Pollutants: VOC

see pdf

A6-65
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: FE-10
Emission Source: Coal Yard Equipment Fueling - 25,000 gallon diesel tank
Pollutants: VOC

see pdf

A6-66
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: FE-11
Emission Source: Ash Haul Truck/Light Vehicle Fueling - 15,000 gallon diesel tank
Pollutants: VOC

see pdf

A6-67
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
EMISSIONS CALCULATIONS

Source Name: FE-12
Emission Source: Ash Haul Truck/Light Vehicle Fueling - 15,000 gallon gasoline tank
Pollutants: VOC

see pdf

A6-68
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
BOILER EMISSIONS (NON-CRITERIA POLLUTANTS)

| | | Maximum Emissions Case (one boiler) | Maximum Emissions Case (two boilers) | Pollutant Form | Pollutant Class | Chemical Abstract Services (CAS) Number |
|--|------------------|---|--|--------------------|--------------------|---|
| PLANT PERFORMANCE: | | | | | | |
| Net Plant Output | Net-kW | 849,756 | 1,699,512 | | | |
| Primary Fuel Feed Rate | Tons/hr | 538 | 1,075 | | | |
| Heat input to Boiler | mmBtu/hr | 8,710 | 17,420 | | | |
| PLANT EMISSION ANALYSIS: | | | | | | |
| Polychlorinated Dibenzo-P-Dioxins and Polychlorinated Dibenzofurans¹ | | | | | | |
| Total TCDD | lb/ton | 3.9E-10 | 3.9E-10 | Particulate | | |
| | lb/hr | 2.1E-07 | 4.2E-07 | | | |
| | tons/year | 9.3E-07 | 1.9E-06 | | | |
| Total PeCDD | lb/ton | 7.1E-10 | 7.1E-10 | Particulate | | |
| | lb/hr | 3.8E-07 | 7.6E-07 | | | |
| | tons/year | 1.7E-06 | 3.3E-06 | | | |
| Total HxCDD | lb/ton | 3.0E-09 | 3.0E-09 | Particulate | | |
| | lb/hr | 1.6E-06 | 3.2E-06 | | | |
| | tons/year | 7.1E-06 | 1.4E-05 | | | |
| Total HpCDD | lb/ton | 1.0E-08 | 1.0E-08 | Particulate | | |
| | lb/hr | 5.4E-06 | 1.1E-05 | | | |
| | tons/year | 2.4E-05 | 4.7E-05 | | | |
| Total OCDD | lb/ton | 2.9E-08 | 2.9E-08 | Particulate | | |
| | lb/hr | 1.5E-05 | 3.1E-05 | | | |
| | tons/year | 6.8E-05 | 1.4E-04 | | | |
| Total PCDD ² | lb/ton | 4.3E-08 | 4.3E-08 | Particulate | | |
| | lb/hr | 2.3E-05 | 4.6E-05 | | | |
| | tons/year | 1.0E-04 | 2.0E-04 | | | |
| Total TCDF | lb/ton | 2.5E-09 | 2.5E-09 | Particulate | | |
| | lb/hr | 1.3E-06 | 2.7E-06 | | | |
| | tons/year | 5.9E-06 | 1.2E-05 | | | |
| Total PeCDF | lb/ton | 4.8E-09 | 4.8E-09 | Particulate | | |
| | lb/hr | 2.6E-06 | 5.2E-06 | | | |
| | tons/year | 1.1E-05 | 2.3E-05 | | | |
| Total HxCDF | lb/ton | 1.3E-08 | 1.3E-08 | Particulate | | |
| | lb/hr | 6.8E-06 | 1.4E-05 | | | |
| | tons/year | 3.0E-05 | 6.0E-05 | | | |
| Total HpCDF | lb/ton | 4.4E-08 | 4.4E-08 | Particulate | | |
| | lb/hr | 2.4E-05 | 4.7E-05 | | | |
| | tons/year | 1.0E-04 | 2.1E-04 | | | |
| Total OCDF | lb/ton | 1.4E-07 | 1.4E-07 | Particulate | | |
| | lb/hr | 7.4E-05 | 1.5E-04 | | | |
| | tons/year | 3.2E-04 | 6.5E-04 | | | |
| Total PCDF ² | lb/ton | 2.0E-07 | 2.0E-07 | Particulate | | |
| | lb/hr | 1.1E-04 | 2.2E-04 | | | |
| | tons/year | 4.7E-04 | 9.5E-04 | | | |
| Total PCDD²/PCDF² | lb/ton | 2.4E-07 | 2.4E-07 | Particulate | | |
| | lb/hr | 1.3E-04 | 2.6E-04 | | | |
| | tons/year | 5.7E-04 | 1.1E-03 | | | |

A6-68
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
BOILER EMISSIONS (NON-CRITERIA POLLUTANTS)

| | | Maximum Emissions Case (one boiler) | Maximum Emissions Case (two boilers) | Pollutant Form | Pollutant Class | Chemical Abstract Services (CAS) Number |
|--------------------------|------------------|---|--|-------------------|--------------------|---|
| PAHs³ | | | | | | |
| Acenaphthene | lb/ton | 5.1E-07 | 5.1E-07 | Particulate | Organic | 83-32-9 |
| | lb/hr | 2.7E-04 | 5.5E-04 | | | |
| | tons/year | 1.2E-03 | 2.4E-03 | | | |
| Acenaphthylene | lb/ton | 2.5E-07 | 2.5E-07 | Particulate | Organic | 208-96-8 |
| | lb/hr | 1.3E-04 | 2.7E-04 | | | |
| | tons/year | 5.9E-04 | 1.2E-03 | | | |
| Anthracene | lb/ton | 2.1E-07 | 2.1E-07 | Particulate | Organic | 120-12-7 |
| | lb/hr | 1.1E-04 | 2.3E-04 | | | |
| | tons/year | 4.9E-04 | 9.9E-04 | | | |
| Benzo(a)anthracene | lb/ton | 8.0E-08 | 8.0E-08 | Particulate | Organic | 56-55-3 |
| | lb/hr | 4.3E-05 | 8.6E-05 | | | |
| | tons/year | 1.9E-04 | 3.8E-04 | | | |
| Benzo(a)pyrene | lb/ton | 3.8E-08 | 3.8E-08 | Particulate | Organic | 50-32-8 |
| | lb/hr | 2.0E-05 | 4.1E-05 | | | |
| | tons/year | 8.9E-05 | 1.8E-04 | | | |
| Benzo(b,j,k)fluoranthene | lb/ton | 1.1E-07 | 1.1E-07 | Particulate | Organic | 205-99-2, 205-82-3, 207-08-9 |
| | lb/hr | 5.9E-05 | 1.2E-04 | | | |
| | tons/year | 2.6E-04 | 5.2E-04 | | | |
| Benzo(g,h,i)perylene | lb/ton | 2.7E-08 | 2.7E-08 | Particulate | Organic | 191-24-2 |
| | lb/hr | 1.5E-05 | 2.9E-05 | | | |
| | tons/year | 6.4E-05 | 1.3E-04 | | | |
| Chrysene | lb/ton | 1.0E-07 | 1.0E-07 | Particulate | Organic | 218-01-9 |
| | lb/hr | 5.4E-05 | 1.1E-04 | | | |
| | tons/year | 2.4E-04 | 4.7E-04 | | | |
| Fluoranthene | lb/ton | 7.1E-07 | 7.1E-07 | Particulate | Organic | 206-44-0 |
| | lb/hr | 3.8E-04 | 7.6E-04 | | | |
| | tons/year | 1.7E-03 | 3.3E-03 | | | |
| Fluorene | lb/ton | 9.1E-07 | 9.1E-07 | Particulate | Organic | 86-73-7 |
| | lb/hr | 4.9E-04 | 9.8E-04 | | | |
| | tons/year | 2.1E-03 | 4.3E-03 | | | |
| Indeno(1,2,3-cd)pyrene | lb/ton | 6.1E-08 | 6.1E-08 | Particulate | Organic | 193-39-5 |
| | lb/hr | 3.3E-05 | 6.6E-05 | | | |
| | tons/year | 1.4E-04 | 2.9E-04 | | | |
| 5-Methyl chrysene | lb/ton | 2.2E-08 | 2.2E-08 | Particulate | Organic | 3697-24-3 |
| | lb/hr | 1.2E-05 | 2.4E-05 | | | |
| | tons/year | 5.2E-05 | 1.0E-04 | | | |
| Phenanthrene | lb/ton | 2.7E-06 | 2.7E-06 | Particulate | Organic | 85-01-8 |
| | lb/hr | 1.5E-03 | 2.9E-03 | | | |
| | tons/year | 6.4E-03 | 1.3E-02 | | | |
| Pyrene | lb/ton | 3.3E-07 | 3.3E-07 | Particulate | Organic | 129-00-0 |
| | lb/hr | 1.8E-04 | 3.5E-04 | | | |
| | tons/year | 7.8E-04 | 1.6E-03 | | | |
| Total PAH | | | | | | |
| | lb/hr | 3.3E-03 | 6.5E-03 | | | |
| | tons/year | 1.4E-02 | 2.9E-02 | | | |

A6-68
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
BOILER EMISSIONS (NON-CRITERIA POLLUTANTS)

| | | Maximum Emissions Case (one boiler) | Maximum Emissions Case (two boilers) | Pollutant Form | Pollutant Class | Chemical Abstract Services (CAS) Number |
|--|------------------------------|---|--|-------------------|--------------------|---|
| Organic HAPs⁴ | | | | | | |
| Acetaldehyde | lb/ton lb/hr tons/year | 5.7E-04 0.306 1.342 | 5.7E-04 0.613 2.685 | Vapor | Organic | 75-07-0 |
| Acetophenone | lb/ton lb/hr tons/year | 1.5E-05 0.008 0.035 | 1.5E-05 0.016 0.071 | Vapor | Organic | 98-86-2 |
| Acrolein | lb/ton lb/hr tons/year | 2.9E-04 0.156 0.683 | 2.9E-04 0.312 1.366 | Vapor | Organic | 107-02-8 |
| Benzene | lb/ton lb/hr tons/year | 1.3E-03 0.699 3.061 | 1.3E-03 1.398 6.123 | Vapor | Organic | 71-43-2 |
| Benzyl chloride | lb/ton lb/hr tons/year | 7.0E-04 0.376 1.648 | 7.0E-04 0.753 3.297 | Vapor | Organic | 100-44-7 |
| Biphenyl (also PAH, not included in total PAHs) | lb/ton lb/hr tons/year | 1.7E-06 9.1E-04 4.0E-03 | 1.7E-06 1.8E-03 8.0E-03 | Vapor | Organic | 92-52-4 |
| Bis(2-ethylhexyl)phthalate (DEHP) | lb/ton lb/hr tons/year | 7.3E-05 0.039 0.172 | 7.3E-05 0.078 0.344 | Particulate | Organic | 117-81-7 |
| Bromoform | lb/ton lb/hr tons/year | 3.9E-05 0.021 0.092 | 3.9E-05 0.042 0.184 | Vapor | Organic | 75-25-2 |
| Carbon disulfide | lb/ton lb/hr tons/year | 1.3E-04 0.070 0.306 | 1.3E-04 0.140 0.612 | Vapor | Inorganic | 75-15-0 |
| 2-Chloroacetophenone | lb/ton lb/hr tons/year | 7.0E-06 3.8E-03 1.6E-02 | 7.0E-06 7.5E-03 3.3E-02 | Particulate | Organic | 532-27-4 |
| Chlorobenzene | lb/ton lb/hr tons/year | 2.2E-05 1.2E-02 0.052 | 2.2E-05 2.4E-02 0.104 | Vapor | Organic | 108-90-7 |
| Chloroform | lb/ton lb/hr tons/year | 5.9E-05 0.032 0.139 | 5.9E-05 0.063 0.278 | Vapor | Organic | 67-66-3 |
| Cumene | lb/ton lb/hr tons/year | 5.3E-06 2.8E-03 1.2E-02 | 5.3E-06 5.7E-03 2.5E-02 | Vapor | Organic | 98-82-8 |
| Cyanide (no longer a HAP, not included in total) | lb/ton lb/hr tons/year | 2.5E-03 1.3E+00 5.887 | 2.5E-03 2.7E+00 11.775 | Vapor | Organic | 77-78-1 |
| Dimethyl sulfate | lb/ton lb/hr tons/year | 4.8E-05 2.6E-02 0.113 | 4.8E-05 5.2E-02 0.226 | Vapor | Organic | 77-78-1 |

A6-68
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
BOILER EMISSIONS (NON-CRITERIA POLLUTANTS)

| | | Maximum Emissions Case (one boiler) | Maximum Emissions Case (two boilers) | Pollutant Form | Pollutant Class | Chemical Abstract Services (CAS) Number |
|--|-----------|---|--|-------------------|--------------------|---|
| 2,4-Dinitrotoluene | lb/ton | 2.8E-07 | 2.8E-07 | Particulate | Organic | 121-14-2 |
| | lb/hr | 1.5E-04 | 3.0E-04 | | | |
| | tons/year | 6.6E-04 | 1.3E-03 | | | |
| Ethyl benzene | lb/ton | 9.4E-05 | 9.4E-05 | Vapor | Organic | 100-41-4 |
| | lb/hr | 0.051 | 0.101 | | | |
| | tons/year | 0.221 | 0.443 | | | |
| Ethyl chloride | lb/ton | 4.2E-05 | 4.2E-05 | Vapor | Organic | 75-00-3 |
| | lb/hr | 2.3E-02 | 4.5E-02 | | | |
| | tons/year | 0.099 | 0.198 | | | |
| Ethylene dichloride | lb/ton | 4.0E-05 | 4.0E-05 | Vapor | Organic | 107-06-2 |
| | lb/hr | 2.2E-02 | 4.3E-02 | | | |
| | tons/year | 0.094 | 0.188 | | | |
| Ethylene dibromide | lb/ton | 1.2E-06 | 1.2E-06 | Vapor | Organic | 106-93-4 |
| | lb/hr | 6.5E-04 | 1.3E-03 | | | |
| | tons/year | 2.8E-03 | 5.7E-03 | | | |
| Formaldehyde | lb/ton | 2.4E-04 | 2.4E-04 | Vapor | Organic | 50-00-0 |
| | lb/hr | 0.129 | 0.258 | | | |
| | tons/year | 0.565 | 1.130 | | | |
| Hexane | lb/ton | 6.7E-05 | 6.7E-05 | Vapor | Organic | 110-54-3 |
| | lb/hr | 0.036 | 0.072 | | | |
| | tons/year | 0.158 | 0.316 | | | |
| Isophorone | lb/ton | 5.8E-04 | 5.8E-04 | Vapor | Organic | 78-59-1 |
| | lb/hr | 0.312 | 0.624 | | | |
| | tons/year | 1.366 | 2.732 | | | |
| Methyl bromide | lb/ton | 1.6E-04 | 1.6E-04 | Vapor | Organic | 74-83-9 |
| | lb/hr | 0.086 | 0.172 | | | |
| | tons/year | 0.377 | 0.754 | | | |
| Methyl chloride | lb/ton | 5.3E-04 | 5.3E-04 | Vapor | Organic | 74-87-3 |
| | lb/hr | 0.285 | 0.570 | | | |
| | tons/year | 1.248 | 2.496 | | | |
| Methyl ethyl ketone (no longer a HAP, not included in total) | lb/ton | 3.9E-04 | 3.9E-04 | Vapor | Organic | 74-87-3 |
| | lb/hr | 0.210 | 0.419 | | | |
| | tons/year | 0.918 | 1.837 | | | |
| Methyl hydrazine | lb/ton | 1.7E-04 | 1.7E-04 | Vapor | Organic | 60-34-4 |
| | lb/hr | 0.091 | 0.183 | | | |
| | tons/year | 0.400 | 0.801 | | | |
| Methyl methacrylate | lb/ton | 2.0E-05 | 2.0E-05 | Vapor | Organic | 80-62-6 |
| | lb/hr | 1.1E-02 | 2.2E-02 | | | |
| | tons/year | 0.047 | 0.094 | | | |
| Methyl tert butyl ether | lb/ton | 3.5E-05 | 3.5E-05 | Vapor | Organic | 1634-04-4 |
| | lb/hr | 1.9E-02 | 3.8E-02 | | | |
| | tons/year | 0.082 | 0.165 | | | |
| Methylene chloride | lb/ton | 2.9E-04 | 2.9E-04 | Vapor | Organic | 75-09-2 |
| | lb/hr | 0.156 | 0.312 | | | |
| | tons/year | 0.236 | 0.236 | | | |

A6-68
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
BOILER EMISSIONS (NON-CRITERIA POLLUTANTS)

| | | Maximum Emissions Case (one boiler) | Maximum Emissions Case (two boilers) | Pollutant Form | Pollutant Class | Chemical Abstract Services (CAS) Number |
|--|------------------|---|--|-------------------|--------------------|---|
| Naphthalene (also PAH, not included in total PAHs) | lb/ton | 1.3E-05 | 1.3E-05 | Particulate | Organic | 91-20-3 |
| | lb/hr | 7.0E-03 | 1.4E-02 | | | |
| | tons/year | 3.1E-02 | 6.1E-02 | | | |
| Phenol | lb/ton | 1.6E-05 | 1.6E-05 | Vapor | Organic | 108-95-2 |
| | lb/hr | 8.6E-03 | 1.7E-02 | | | |
| | tons/year | 0.038 | 0.075 | | | |
| Propionaldehyde | lb/ton | 3.8E-04 | 3.8E-04 | Vapor | Organic | 123-38-6 |
| | lb/hr | 0.204 | 0.409 | | | |
| | tons/year | 0.895 | 1.790 | | | |
| Styrene | lb/ton | 2.5E-05 | 2.5E-05 | Vapor | Organic | 100-42-5 |
| | lb/hr | 1.3E-02 | 2.7E-02 | | | |
| | tons/year | 0.059 | 0.118 | | | |
| Tetrachloroethylene | lb/ton | 4.3E-05 | 4.3E-05 | Vapor | Organic | 127-18-4 |
| | lb/hr | 2.3E-02 | 4.6E-02 | | | |
| | tons/year | 0.101 | 0.203 | | | |
| Toluene | lb/ton | 2.4E-04 | 2.4E-04 | Vapor | Organic | 108-88-3 |
| | lb/hr | 0.129 | 0.258 | | | |
| | tons/year | 0.565 | 1.130 | | | |
| 1,1,1-Trichloroethane (Methyl chloroform) | lb/ton | 2.0E-05 | 2.0E-05 | Vapor | Organic | 71-55-6 |
| | lb/hr | 1.1E-02 | 2.2E-02 | | | |
| | tons/year | 0.047 | 0.094 | | | |
| Vinyl acetate | lb/ton | 7.6E-06 | 7.6E-06 | Vapor | Organic | 108-05-4 |
| | lb/hr | 4.1E-03 | 8.2E-03 | | | |
| | tons/year | 1.8E-02 | 3.6E-02 | | | |
| Xylenes | lb/ton | 3.7E-05 | 3.7E-05 | Vapor | Organic | 1330-20-7 |
| | lb/hr | 2.0E-02 | 4.0E-02 | | | |
| | tons/year | 0.087 | 0.174 | | | |
| Total Organic HAPs | lb/hr | 3.4 | 6.8 | | | |
| | tons/year | 14.4 | 28.6 | | | |

A6-68
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
BOILER EMISSIONS (NON-CRITERIA POLLUTANTS)

| | | Maximum Emissions Case (one boiler) | Maximum Emissions Case (two boilers) | Pollutant Form | Pollutant Class | Chemical Abstract Services (CAS) Number |
|-----------------------------------|---|---|--|-----------------------|--------------------|---|
| Inorganic HAPs⁵ | | | | | | |
| Antimony | lb/ton lb/hr tons/year | 1.8E-05 0.010 0.042 | 1.8E-05 0.019 0.085 | Particulate | Inorganic | 7440-36-0 |
| Arsenic | lb/ton lb/hr tons/year | 4.1E-04 0.220 0.966 | 4.1E-04 0.441 1.931 | Particulate | Inorganic | 7440-38-2 |
| Beryllium | lb/ton lb/hr tons/year | 2.1E-05 0.011 0.049 | 2.1E-05 0.023 0.099 | Particulate | Inorganic | 7440-41-7 |
| Cadmium | lb/ton lb/hr tons/year | 5.1E-05 0.027 0.120 | 5.1E-05 0.055 0.240 | Particulate | Inorganic | 7440-43-9 |
| Chromium | lb/ton lb/hr tons/year | 2.6E-04 0.140 0.612 | 2.6E-04 0.280 1.225 | Particulate | Inorganic | 7440-47-3 |
| Chromium (VI) | lb/ton lb/hr tons/year | 7.9E-05 0.042 0.186 | 7.9E-05 0.085 0.372 | Particulate | Inorganic | 18540-29-9 |
| Cobalt | lb/ton lb/hr tons/year | 1.0E-04 0.054 0.235 | 1.0E-04 0.108 0.471 | Particulate | Inorganic | 7440-48-4 |
| Hydrogen chloride ⁶ | lb/ton control (%) lb/hr tons/year | 1.2E+00 85.0% 9.678E+01 423.9 | 1.2E+00 85.0% 1.9E+02 847.8 | Vapor | Inorganic | 7647-01-0 |
| Hydrogen fluoride ⁷ | lb/mmBtu lb/hr tons/year | 4.0E-04 3.5 15.3 | 4.0E-04 7.0 30.5 | Vapor | Inorganic | 73602-61-6 |
| Lead | lb/ton lb/hr tons/year | 4.2E-04 0.226 0.989 | 4.2E-04 0.452 1.978 | Particulate | Inorganic | 7439-92-1 |
| Manganese | lb/ton lb/hr tons/year | 4.9E-04 0.263 1.154 | 4.9E-04 0.527 2.308 | Particulate | Inorganic | 7439-96-5 |
| Mercury ⁸ | lb/MWh lb/hr tons/year | 2.00E-05 0.017 0.074 | 2.00E-05 0.034 0.149 | Vapor/ Particulate | Inorganic | 7439-97-6 |
| Nickel | lb/ton lb/hr tons/year | 2.8E-04 0.151 0.659 | 2.8E-04 0.301 1.319 | Particulate | Inorganic | 7440-02-0 |
| Selenium | lb/ton lb/hr tons/year | 1.3E-03 0.699 3.061 | 1.3E-03 1.398 6.123 | Particulate | Inorganic | 7782-49-2 |
| Total Inorganic HAPs | lb/hr tons/year | 102.1 447.3 | 204.2 894.6 | | | |

A6-68
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
BOILER EMISSIONS (NON-CRITERIA POLLUTANTS)

| | | Maximum Emissions Case (one boiler) | Maximum Emissions Case (two boilers) | Pollutant Form | Pollutant Class | Chemical Abstract Services (CAS) Number |
|-------------------|------------------|---|--|-------------------|--------------------|---|
| Total HAPs | lb/hr | 105.5 | 211.0 | | | |
| | tons/year | 461.7 | 923.2 | | | |

STACK PARAMETERS:

| | | | |
|--|-----------|--|---------------------|
| Stack Flue Gas Temperature | 324 | K | |
| Stack Flue Gas Flow Rate | 3,382,914 | acfm | |
| Stack Flue Gas Flow Rate | 2,246,137 | scfm | |
| Exit Velocity | 55 | ft/s at 100% (assume velocity is at actual conditions) | |
| Height | 727 | ft | |
| Stack diameter (top ID) | 36 | ft | (each boiler stack) |
| Stack top area | 1,023 | ft ² | |
| Ash Content | 13 | % | |
| Moisture Content | 27.00 | % | |
| Filterable PM ₁₀ emissions factor | 0.010 | lb/mmBtu | |

Notes:

- ¹ Emission factors for Polychlorinated Dibenzo-p-dioxins and Polychlorinated Dibenzofurans were found in AP-42 Table 1.1-12 "Emission Factors for Polychlorinated Dibenzo-p-dioxins and Polychlorinated Dibenzofurans From Controlled Bituminous and Sub-bituminous Coal Combustion"
- ² Total PCDD is the sum of Total TCDD through Total OCDD. Total PCDF is the sum of Total TCDF through Total OCDF.
- ³ Emission factors for Polynuclear Aromatic Hydrocarbons were found in AP-42 Table 1.1-13 "Emission Factors for Polynuclear Aromatic Hydrocarbons From Controlled Coal Combustion"
- ⁴ Emission factors for Organic HAPs and other compounds were found in AP-42 Table 1.1-14 "Emission Factors for Various Organic Compounds From Controlled Coal Combustion"
- ⁵ Emission factors for Trace Metals were found in AP-42 Table 1.1-18 "Emission Factors for Trace Metals From Controlled Coal Combustion"
- ⁶ Emission factors for HCl were found in AP-42 Table 1.1-15 "Emission Factors for Hydrogen Chloride and Hydrogen Fluoride from Coal Combustion". Control efficiency of 85% for wet scrubber and baghouse per Sierra Pacific Power Company.
- ⁷ Per Cummins & Barnard
- ⁸ 20 E -6 lb/ MWh per Carl Weilert review of proposed Nevada Regulation R162-06: Clean Air Mercury Rule (CAMR) per Burns and McDonald.

A6-69
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
AUXILIARY BOILER EMISSIONS NON-CRITERIA POLLUTANTS

| Pollutant | Emission Factor | Units | Source | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Pollutant Form | Pollutant Class | Chemical Abstract Services (CAS) Number |
|-----------------------------|-----------------|-------------------------|------------------------------|--------------------------|---------------------------|------------------------|-----------------|---|
| Organic HAPs | | | | | | | | |
| Formaldehyde ¹ | 6.10E-02 | lb/10 ³ Gal | AP-42 (9/98) Table 1.3-8 | 9.59E-02 | 4.20E-01 | Vapor | Organic | 50-00-0 |
| Total Organic HAPs | | | | 9.59E-02 | 4.20E-01 | | | |
| Inorganic HAPs | | | | | | | | |
| Arsenic | 4 | lb/10 ¹² Btu | AP-42 (9/98) Table 1.3-10 | 8.80E-04 | 3.85E-03 | Particulate | Inorganic | 7440-38-2 |
| Beryllium | 3 | lb/10 ¹² Btu | AP-42 (9/98) Table 1.3-10 | 6.60E-04 | 2.89E-03 | Particulate | Inorganic | 7440-41-7 |
| Cadmium | 3 | lb/10 ¹² Btu | AP-42 (9/98) Table 1.3-10 | 6.60E-04 | 2.89E-03 | Particulate | Inorganic | 7440-43-9 |
| Chromium | 3 | lb/10 ¹² Btu | AP-42 (9/98) Table 1.3-10 | 6.60E-04 | 2.89E-03 | Particulate | Inorganic | 7440-47-3 |
| Lead | 9 | lb/10 ¹² Btu | AP-42 (9/98) Table 1.3-10 | 1.98E-03 | 8.67E-03 | Particulate | Inorganic | 7439-92-1 |
| Manganese | 6 | lb/10 ¹² Btu | AP-42 (9/98) Table 1.3-10 | 1.32E-03 | 5.78E-03 | Particulate | Inorganic | 7439-96-5 |
| Mercury | 3 | lb/10 ¹² Btu | AP-42 (9/98) Table 1.3-10 | 6.60E-04 | 2.89E-03 | Vapor/ Particulates | Inorganic | 7439-97-6 |
| Nickel | 3 | lb/10 ¹² Btu | AP-42 (9/98) Table 1.3-10 | 6.60E-04 | 2.89E-03 | Particulate | Inorganic | 7440-02-0 |
| Selenium | 15 | lb/10 ¹² Btu | AP-42 (9/98) Table 1.3-10 | 3.30E-03 | 1.45E-02 | Particulate | Inorganic | 7782-49-2 |
| Total Inorganic HAPs | | | | 1.08E-02 | 4.72E-02 | | | |
| Total HAPs | | | | 1.07E-01 | 4.67E-01 | | | |
| Other Pollutants | | | | | | | | |
| Copper | 6 | lb/10 ¹² Btu | AP-42 (9/98) Table 1.3-10 | 1.32E-03 | 5.78E-03 | Particulate | Inorganic | 7440-50-8 |
| Zinc | 4 | lb/10 ¹² Btu | AP-42 (9/98) Table 1.3-10 | 8.80E-04 | 3.85E-03 | Particulate | Inorganic | 7440-66-6 |

| | |
|------------------------|---------|
| Sulfur Content of Fuel | 0.0015% |
|------------------------|---------|

STACK PARAMETERS:

| | | | |
|----------------------------|--------|-----------------|---------|
| Stack Flue Gas Temperature | 350 | °F | 449.8 K |
| Stack Flue Gas Flow Rate | 69,208 | acfm | |
| Stack Flue Gas Flow Rate | 33,129 | scfm | |
| Exit Velocity | 59.06 | ft/sec | |
| Height | 299.87 | ft | |
| Stack diameter (top ID) | 4.99 | ft | |
| Stack area | 19.53 | ft ² | |

| | | |
|--|---------|------------|
| Maximum Fuel Firing Rate for Auxiliary Boiler: | 220.0 | mmBtu/hr |
| Heating Value for propane Fuel: | 140,000 | Btu/gal |
| Maximum Fuel Firing Rate: | 1571.43 | gal/hr |
| Estimated Maximum Annual Hours of Operation: | 8,760 | hours/year |

Note:

1 - The emission factor for formaldehyde was obtained from AP-42 Table 1.3-8. This table provides a range for the emission factor of 0.035 to 0.061 lb/103 gal for distillate oil fired utility/industrial/commercial boilers. The higher emission factor was chosen for the calculation for conservatism.

Stack height of Auxiliary Boiler is assumed to be 10 ft above height of boiler buildings

Boiler heat input is assumed to be 140,000 lb/hr steam with 15% margin.

A6-70
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
PLANT DIESEL ENGINE AUXILIARY GENERATOR EMISSIONS NON-CRITERIA POLLUTANTS

| Pollutant | Emission Factor | Units | Source | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Pollutant Form | Pollutant Class | Chemical Abstract Services (CAS) Number |
|---------------------------|-----------------|----------|------------------------------|--------------------------|---------------------------|----------------|-----------------|---|
| PAHs | | | | | | | | |
| Acenaphthene | 4.68E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 8.91E-05 | 1.11E-05 | Particulate | Organic | 83-32-9 |
| Acenaphthylene | 9.23E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.76E-04 | 2.20E-05 | Particulate | Organic | 208-96-8 |
| Anthracene | 1.23E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 2.34E-05 | 2.93E-06 | Particulate | Organic | 120-12-7 |
| Benzo(a)anthracene | 6.22E-07 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.18E-05 | 1.48E-06 | Particulate | Organic | 56-55-3 |
| Benzo(a)pyrene | 2.57E-07 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 4.89E-06 | 6.11E-07 | Particulate | Organic | 50-32-8 |
| Benzo(b)fluoranthene | 1.11E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 2.11E-05 | 2.64E-06 | Particulate | Organic | 205-99-2 |
| Benzo(k)fluoranthene | 2.18E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 4.15E-05 | 5.19E-06 | Particulate | Organic | 207-08-9 |
| Benzo(g,h,i)perylene | 5.56E-07 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.06E-05 | 1.32E-06 | Particulate | Organic | 205-82-3, 207-08-9 |
| Chrysene | 1.53E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 2.91E-05 | 3.64E-06 | Particulate | Organic | 218-01-9 |
| Dibenz(a,h)anthracene | 3.46E-07 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 6.59E-06 | 8.23E-07 | Particulate | Organic | 53-70-3 |
| Fluoranthene | 4.03E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 7.67E-05 | 9.59E-06 | Particulate | Organic | 206-44-0 |
| Fluorene | 1.28E-05 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 2.44E-04 | 3.05E-05 | Particulate | Organic | 86-73-7 |
| Indeno(1,2,3-cd)pyrene | 4.14E-07 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 7.88E-06 | 9.85E-07 | Particulate | Organic | 193-39-5 |
| Phenanthrene | 4.08E-05 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 7.77E-04 | 9.71E-05 | Particulate | Organic | 85-01-8 |
| Pyrene | 3.71E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 7.06E-05 | 8.83E-06 | Particulate | Organic | 129-00-0 |
| Total PAH | 8.35E-05 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.59E-03 | 1.99E-04 | | Organic | |
| Organic HAPs | | | | | | | | |
| Acetaldehyde | 2.52E-05 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 4.80E-04 | 6.00E-05 | Vapor | Organic | 75-07-0 |
| Acrolein | 7.88E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 1.50E-04 | 1.87E-05 | Vapor | Organic | 107-02-8 |
| Benzene | 7.76E-04 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 1.48E-02 | 1.85E-03 | Vapor | Organic | 71-43-2 |
| Formaldehyde | 7.89E-05 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 1.50E-03 | 1.88E-04 | Vapor | Organic | 50-00-0 |
| Naphthalene | 1.30E-04 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 2.47E-03 | 3.09E-04 | Particulate | Organic | 91-20-3 |
| Propylene | 2.79E-03 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 5.31E-02 | 6.64E-03 | Particulate | Organic | 115-07-1 |
| Toluene | 2.81E-04 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 5.35E-03 | 6.69E-04 | Vapor | Organic | 108-88-3 |
| Xylenes | 1.93E-04 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 3.67E-03 | 4.59E-04 | Vapor | Organic | 1330-20-7 |
| Total Organic HAPs | 4.28E-03 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 8.15E-02 | 1.02E-02 | | Organic | |

A6-70
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
PLANT DIESEL ENGINE AUXILIARY GENERATOR EMISSIONS NON-CRITERIA POLLUTANTS

| | |
|------------------------|---------|
| Sulfur Content of Fuel | 0.0015% |
|------------------------|---------|

Description: Emission estimates based on a 750 kW emergency diesel generator using No. 2 fuel oil.
The calculations are based on AP-42 emission factors except as noted.

STACK PARAMETERS:

| | | | |
|------------------------------------|--------|-----------------|-------------------|
| Stack Flue Gas Temperature | 711 | K | |
| Flow Rate | 56,871 | acfm | |
| Flow Rate | 17,225 | scfm | |
| Exit Velocity | 72.20 | ft/sec | |
| Height | 19.98 | ft | |
| Stack diameter (top ID) | 27.00 | inch | |
| Stack area | 3.98 | ft ² | |
| Diesel engine output: | 4650 | hp | |
| Diesel engine output: | 11.84 | mmBtu/hr | 1hp = 2546 Btu/hr |
| Diesel engine input: | 138.9 | gal/hr | 19.0 mmBtu/hr |
| Maximum Annual Hours of Operation: | 250 | hours/year | |

Notes:

No Inorganic HAPs according to AP-42, Section 3.4

Stack heights, temperatures, velocities, and diameters and fuel usage rates obtained from Caterpillar data sheets.

Diesel engine input value in mmBtu/hr is based on the assumption the heating value of diesel fuel is 19,300 Btu/lb with a fuel density of 7.1 lb/gal, using the fuel usage value of 138.9 gal/hr.

A6-71
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
DIESEL FIRE WATER PUMP EMISSIONS NON-CRITERIA POLLUTANTS

| Pollutant | Emission Factor | Units | Source | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Pollutant Form | Pollutant Class | Chemical Abstract Services (CAS) Number |
|---------------------------|-----------------|----------|------------------------------|--------------------------|---------------------------|----------------|-----------------|---|
| PAHs | | | | | | | | |
| Acenaphthene | 1.42E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 8.17E-07 | 1.02E-07 | Particulate | Organic | 83-32-9 |
| Acenaphthylene | 5.06E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.91E-06 | 3.64E-07 | Particulate | Organic | 208-96-8 |
| Anthracene | 1.87E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.08E-06 | 1.35E-07 | Particulate | Organic | 120-12-7 |
| Benzo(a)anthracene | 1.68E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 9.67E-07 | 1.21E-07 | Particulate | Organic | 56-55-3 |
| Benzo(a)pyrene | 1.88E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.08E-07 | 1.35E-08 | Particulate | Organic | 50-32-8 |
| Benzo(b)fluoranthene | 9.91E-08 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 5.70E-08 | 7.13E-09 | Particulate | Organic | 205-99-2 |
| Benzo(k)fluoranthene | 1.55E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 8.92E-08 | 1.12E-08 | Particulate | Organic | 207-08-9 |
| Benzo(g,h,i)perylene | 4.89E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.81E-07 | 3.52E-08 | Particulate | Organic | 191-24-2 |
| Chrysene | 3.53E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.03E-07 | 2.54E-08 | Particulate | Organic | 218-01-9 |
| Dibenz(a,h)anthracene | 5.83E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 3.36E-07 | 4.19E-08 | Particulate | Organic | 53-70-3 |
| Fluoranthene | 7.61E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 4.38E-06 | 5.47E-07 | Particulate | Organic | 206-44-0 |
| Fluorene | 2.92E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.68E-05 | 2.10E-06 | Particulate | Organic | 86-73-7 |
| Indeno(1,2,3-cd)pyrene | 3.75E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.16E-07 | 2.70E-08 | Particulate | Organic | 193-39-5 |
| Phenanthrene | 2.94E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.69E-05 | 2.12E-06 | Particulate | Organic | 85-01-8 |
| Pyrene | 4.78E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.75E-06 | 3.44E-07 | Particulate | Organic | 129-00-0 |
| Total PAH | 8.33E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 4.79E-05 | 5.99E-06 | | Organic | |
| Organic HAPs | | | | | | | | |
| Acetaldehyde | 7.67E-04 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 4.41E-04 | 5.52E-05 | Vapor | Organic | 75-07-0 |
| Acrolein | 9.25E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 5.32E-05 | 6.65E-06 | Vapor | Organic | 107-02-8 |
| Benzene | 9.33E-04 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 5.37E-04 | 6.71E-05 | Vapor | Organic | 71-43-2 |
| 1,3-Butadiene | 3.91E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.25E-05 | 2.81E-06 | Vapor | Organic | 106-99-0 |
| Formaldehyde | 1.18E-03 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 6.79E-04 | 8.49E-05 | Vapor | Organic | 50-00-0 |
| Naphthalene | 8.48E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 4.88E-05 | 6.10E-06 | Particulate | Organic | 91-20-3 |
| Propylene | 2.58E-03 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.48E-03 | 1.86E-04 | Particulate | Organic | 115-07-1 |
| Toluene | 4.09E-04 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.35E-04 | 2.94E-05 | Vapor | Organic | 108-88-3 |
| Xylenes | 2.85E-04 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.64E-04 | 2.05E-05 | Vapor | Organic | 1330-20-7 |
| Total Organic HAPs | 6.37E-03 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 3.67E-03 | 4.58E-04 | | Organic | |

A6-71
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
DIESEL FIRE WATER PUMP EMISSIONS NON-CRITERIA POLLUTANTS

| | |
|------------------------|---------|
| Sulfur Content of Fuel | 0.0015% |
|------------------------|---------|

Description: Emission estimates are for a 787.5 HP diesel driven fire pump.
Calculations are based on AP-42 emission factors.

STACK PARAMETER

| | | | | |
|------------------------------------|--------|-----------------|-----------------|----------|
| Stack Flue Gas Temperature | 836 | K | | |
| Flow Rate | 15,970 | acfm | | |
| Flow Rate | 4,111 | scfm | | |
| Exit Velocity | 87 | ft/sec | | |
| Height | 10 | ft | | |
| Stack diameter (top ID) | 12 | inch | | |
| Stack area | 1 | ft ² | | |
| Diesel engine output: | 788 | HP | 1hp=2546 Btu/hr | |
| Diesel engine output: | 2.00 | mmBtu/hr | | |
| Diesel engine input: | 4.2 | gal/hr | 0.6 | mmBtu/hr |
| Maximum Annual Hours of Operation: | 250 | hours/year | | |

Notes:

No Inorganic HAPs according to AP-42, Section 3.3

Diesel engine input value in mmBtu/hr is based on the assumption the heating value of diesel fuel is 19,300 lb/hr with a fuel density of 7.1 lb/gal, using the fuel usage value of 4.2 gal/hr.

A6-72
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
DIESEL BOOSTER FIRE PUMP EMISSIONS NON-CRITERIA POLLUTANTS

| Pollutant | Emission Factor | Units | Source | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Pollutant Form | Pollutant Class | Chemical Abstract Services (CAS) Number |
|---------------------------|-----------------|----------|------------------------------|--------------------------|---------------------------|----------------|-----------------|---|
| PAHs | | | | | | | | |
| Acenaphthene | 1.42E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 8.17E-07 | 1.02E-07 | Particulate | Organic | 83-32-9 |
| Acenaphthylene | 5.06E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.91E-06 | 3.64E-07 | Particulate | Organic | 208-96-8 |
| Anthracene | 1.87E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.08E-06 | 1.35E-07 | Particulate | Organic | 120-12-7 |
| Benzo(a)anthracene | 1.68E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 9.67E-07 | 1.21E-07 | Particulate | Organic | 56-55-3 |
| Benzo(a)pyrene | 1.88E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.08E-07 | 1.35E-08 | Particulate | Organic | 50-32-8 |
| Benzo(b)fluoranthene | 9.91E-08 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 5.70E-08 | 7.13E-09 | Particulate | Organic | 205-99-2 |
| Benzo(k)fluoranthene | 1.55E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 8.92E-08 | 1.12E-08 | Particulate | Organic | 207-08-9 |
| Benzo(g,h,i)perylene | 4.89E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.81E-07 | 3.52E-08 | Particulate | Organic | 191-24-2 |
| Chrysene | 3.53E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.03E-07 | 2.54E-08 | Particulate | Organic | 218-01-9 |
| Dibenz(a,h)anthracene | 5.83E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 3.36E-07 | 4.19E-08 | Particulate | Organic | 53-70-3 |
| Fluoranthene | 7.61E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 4.38E-06 | 5.47E-07 | Particulate | Organic | 206-44-0 |
| Fluorene | 2.92E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.68E-05 | 2.10E-06 | Particulate | Organic | 86-73-7 |
| Indeno(1,2,3-cd)pyrene | 3.75E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.16E-07 | 2.70E-08 | Particulate | Organic | 193-39-5 |
| Phenanthrene | 2.94E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.69E-05 | 2.12E-06 | Particulate | Organic | 85-01-8 |
| Pyrene | 4.78E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.75E-06 | 3.44E-07 | Particulate | Organic | 129-00-0 |
| Total PAH | 8.33E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 4.79E-05 | 5.99E-06 | | Organic | |
| Organic HAPs | | | | | | | | |
| Acetaldehyde | 7.67E-04 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 4.41E-04 | 5.52E-05 | Vapor | Organic | 75-07-0 |
| Acrolein | 9.25E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 5.32E-05 | 6.65E-06 | Vapor | Organic | 107-02-8 |
| Benzene | 9.33E-04 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 5.37E-04 | 6.71E-05 | Vapor | Organic | 71-43-2 |
| 1,3-Butadiene | 3.91E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.25E-05 | 2.81E-06 | Vapor | Organic | 106-99-0 |
| Formaldehyde | 1.18E-03 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 6.79E-04 | 8.49E-05 | Vapor | Organic | 50-00-0 |
| Naphthalene | 8.48E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 4.88E-05 | 6.10E-06 | Particulate | Organic | 91-20-3 |
| Propylene | 2.58E-03 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.48E-03 | 1.86E-04 | Particulate | Organic | 115-07-1 |
| Toluene | 4.09E-04 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.35E-04 | 2.94E-05 | Vapor | Organic | 108-88-3 |
| Xylenes | 2.85E-04 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.64E-04 | 2.05E-05 | Vapor | Organic | 1330-20-7 |
| Total Organic HAPs | 6.37E-03 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 3.67E-03 | 4.58E-04 | | Organic | |

A6-72
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
DIESEL BOOSTER FIRE PUMP EMISSIONS NON-CRITERIA POLLUTANTS

| | |
|------------------------|---------|
| Sulfur Content of Fuel | 0.0015% |
|------------------------|---------|

Description: Emission estimates are for a 90 HP diesel driven fire pump.
Calculations are based on AP-42 emission factors.

STACK PARAMETERS:

| | | |
|----------------------------|-------|-----------------|
| Stack Flue Gas Temperature | 308 | K |
| Flow Rate | 518 | acfm |
| Flow Rate | 362 | scfm |
| Exit Velocity | 17.28 | ft/sec |
| Height | 10.00 | ft |
| Stack diameter (top ID) | 8.00 | inch |
| Stack area | 0.35 | ft ² |

| | | | |
|------------------------------------|------|------------|-----------------|
| Diesel engine output: | 90 | HP | 1hp=2546 Btu/hr |
| Diesel engine output: | 0.23 | mmBtu/hr | |
| Diesel engine input: | 4.2 | gal/hr | 0.6 mmBtu/hr |
| Maximum Annual Hours of Operation: | 250 | hours/year | |

Notes:
No Inorganic HAPs according to AP-42, Section 3.3
Diesel engine input value in mmBtu/hr is based on the assumption the heating value of diesel fuel is 19,300 lb/hr with a fuel density of 7.1 lb/gal, using the fuel usage value of 4.2 gal/hr.

A6-73
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
PLANT DIESEL LOCOMOTIVE ENGINE EMISSIONS NON-CRITERIA POLLUTANTS

| | | | | Per Engine ¹ | | Per 6 Engines ¹ | | | | |
|------------------------|-----------------|----------|------------------------------|--------------------------|---------------------------|----------------------------|---------------------------|----------------|-----------------|---|
| Pollutant | Emission Factor | Units | Source | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Pollutant Form | Pollutant Class | Chemical Abstract Services (CAS) Number |
| PAHs | | | | | | | | | | |
| Acenaphthene | 4.68E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 2.23E-05 | 9.77E-05 | 1.34E-04 | 5.86E-04 | Particulate | Organic | 83-32-9 |
| Acenaphthylene | 9.23E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 4.40E-05 | 1.93E-04 | 2.64E-04 | 1.16E-03 | Particulate | Organic | 208-96-8 |
| Anthracene | 1.23E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 5.87E-06 | 2.57E-05 | 3.52E-05 | 1.54E-04 | Particulate | Organic | 120-12-7 |
| Benzo(a)anthracene | 6.22E-07 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 2.97E-06 | 1.30E-05 | 1.78E-05 | 7.79E-05 | Particulate | Organic | 56-55-3 |
| Benzo(a)pyrene | 2.57E-07 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.23E-06 | 5.37E-06 | 7.35E-06 | 3.22E-05 | Particulate | Organic | 50-32-8 |
| Benzo(b)fluoranthene | 1.11E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 5.29E-06 | 2.32E-05 | 3.18E-05 | 1.39E-04 | Particulate | Organic | 205-99-2 |
| Benzo(k)fluoranthene | 2.18E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.04E-05 | 4.55E-05 | 6.24E-05 | 2.73E-04 | Particulate | Organic | 207-08-9 |
| Benzo(g,h,i)perylene | 5.56E-07 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 2.65E-06 | 1.16E-05 | 1.59E-05 | 6.97E-05 | Particulate | Organic | 191-24-2, 205-82-3, 207-08-9 |
| Chrysene | 1.53E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 7.30E-06 | 3.20E-05 | 4.38E-05 | 1.92E-04 | Particulate | Organic | 218-01-9 |
| Dibenz(a,h)anthracene | 3.46E-07 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.65E-06 | 7.23E-06 | 9.90E-06 | 4.34E-05 | Particulate | Organic | 53-70-3 |
| Fluoranthene | 4.03E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.92E-05 | 8.42E-05 | 1.15E-04 | 5.05E-04 | Particulate | Organic | 206-44-0 |
| Fluorene | 1.28E-05 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 6.10E-05 | 2.67E-04 | 3.66E-04 | 1.60E-03 | Particulate | Organic | 86-73-7 |
| Indeno(1,2,3-cd)pyrene | 4.14E-07 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.97E-06 | 8.65E-06 | 1.18E-05 | 5.19E-05 | Particulate | Organic | 193-39-5 |
| Phenanthrene | 4.08E-05 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.95E-04 | 8.52E-04 | 1.17E-03 | 5.11E-03 | Particulate | Organic | 85-01-8 |
| Pyrene | 3.71E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.77E-05 | 7.75E-05 | 1.06E-04 | 4.65E-04 | Particulate | Organic | 129-00-0 |
| Total PAH | 8.35E-05 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 3.98E-04 | 1.74E-03 | 2.39E-03 | 1.05E-02 | | Organic | |
| Organic HAPs | | | | | | | | | | |
| Acetaldehyde | 2.52E-05 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 1.20E-04 | 5.26E-04 | 7.21E-04 | 3.16E-03 | Vapor | Organic | 75-07-0 |
| Acrolein | 7.88E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 3.76E-05 | 1.65E-04 | 2.25E-04 | 9.88E-04 | Vapor | Organic | 107-02-8 |
| Benzene | 7.76E-04 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 3.70E-03 | 1.62E-02 | 2.22E-02 | 9.72E-02 | Vapor | Organic | 71-43-2 |
| Formaldehyde | 7.89E-05 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 3.76E-04 | 1.65E-03 | 2.26E-03 | 9.89E-03 | Vapor | Organic | 50-00-0 |
| Naphthalene | 1.30E-04 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 6.20E-04 | 2.72E-03 | 3.72E-03 | 1.63E-02 | Particulate | Organic | 91-20-3 |
| Propylene | 2.79E-03 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.33E-02 | 5.83E-02 | 7.98E-02 | 3.50E-01 | Particulate | Organic | 115-07-1 |
| Toluene | 2.81E-04 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 1.34E-03 | 5.87E-03 | 8.04E-03 | 3.52E-02 | Vapor | Organic | 108-88-3 |
| Xylenes | 1.93E-04 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 9.20E-04 | 4.03E-03 | 5.52E-03 | 2.42E-02 | Vapor | Organic | 1330-20-7 |
| Total Organic HAPs | 4.28E-03 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 2.04E-02 | 8.94E-02 | 1.23E-01 | 5.37E-01 | | Organic | |

A6-73
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
PLANT DIESEL LOCOMOTIVE ENGINE EMISSIONS NON-CRITERIA POLLUTANTS

| | |
|------------------------|---------|
| Sulfur Content of Fuel | 0.0015% |
|------------------------|---------|

Description: Emission estimates based on a idle diesel locomotive engines using No. 2 fuel oil. The calculations are based on AP-42 emission factors except as noted.

STACK PARAMETERS:

| | | | | |
|------------------------------------|--------|-----------------|-------------------|----------|
| Stack Flue Gas Temperature | 800 | °F | 700 | K |
| Flow Rate | 28,611 | acfm | | |
| Flow Rate | 8,801 | scfm | | |
| Exit Velocity | 83.01 | ft/sec | | |
| Height | 19.98 | ft | | |
| Stack diameter (top ID) | 18.00 | inch | | |
| Stack area | 1.77 | ft ² | | |
| Diesel engine idle output: | 400 | hp | | |
| Diesel engine idle output: | 1.02 | mmBtu/hr | 1hp = 2546 Btu/hr | |
| Diesel engine input: | 34.8 | gal/hr | 4.8 | mmBtu/hr |
| Maximum Annual Hours of Operation: | 8760 | hours/year | | |

Notes:

¹ It is assumed that 6 locomotive engines will be present on-site at one time, 3 in the front of the train, and 3 at the back.

² source: USEPA Final Emission Standards for Locomotives - Tier 1 Line-Haul Duty Cycle Exhaust Emission Standards (EPA 420-F-97-048)

Diesel engine input value in mmBtu/hr is based on the assumption the heating value of diesel fuel is 19,300 Btu/lb with a fuel density of 7.1 lb/gal, using the fuel usage value of 34.8 gal/hr.

A6-74
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
SWITCHYARD DIESEL ENGINE AUXILIARY GENERATOR EMISSIONS NON-CRITERIA POLLUTANTS

| Pollutant | Emission Factor | Units | Source | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Pollutant Form | Pollutant Class | Chemical Abstract Services (CAS) Number |
|---------------------------|-----------------|----------|------------------------------|--------------------------|---------------------------|----------------|-----------------|---|
| PAHs | | | | | | | | |
| Acenaphthene | 4.68E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 2.40E-05 | 3.00E-06 | Particulate | Organic | 83-32-9 |
| Acenaphthylene | 9.23E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 4.73E-05 | 5.91E-06 | Particulate | Organic | 208-96-8 |
| Anthracene | 1.23E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 6.30E-06 | 7.88E-07 | Particulate | Organic | 120-12-7 |
| Benzo(a)anthracene | 6.22E-07 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 3.19E-06 | 3.98E-07 | Particulate | Organic | 56-55-3 |
| Benzo(a)pyrene | 2.57E-07 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.32E-06 | 1.65E-07 | Particulate | Organic | 50-32-8 |
| Benzo(b)fluoranthene | 1.11E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 5.69E-06 | 7.11E-07 | Particulate | Organic | 205-99-2 |
| Benzo(k)fluoranthene | 2.18E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.12E-05 | 1.40E-06 | Particulate | Organic | 207-08-9 |
| Benzo(g,h,i)perylene | 5.56E-07 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 2.85E-06 | 3.56E-07 | Particulate | Organic | 205-82-3, 207-08-9 |
| Chrysene | 1.53E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 7.84E-06 | 9.80E-07 | Particulate | Organic | 218-01-9 |
| Dibenz(a,h)anthracene | 3.46E-07 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.77E-06 | 2.22E-07 | Particulate | Organic | 53-70-3 |
| Fluoranthene | 4.03E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 2.07E-05 | 2.58E-06 | Particulate | Organic | 206-44-0 |
| Fluorene | 1.28E-05 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 6.56E-05 | 8.20E-06 | Particulate | Organic | 86-73-7 |
| Indeno(1,2,3-cd)pyrene | 4.14E-07 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 2.12E-06 | 2.65E-07 | Particulate | Organic | 193-39-5 |
| Phenanthrene | 4.08E-05 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 2.09E-04 | 2.61E-05 | Particulate | Organic | 85-01-8 |
| Pyrene | 3.71E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.90E-05 | 2.38E-06 | Particulate | Organic | 129-00-0 |
| Total PAH | 8.35E-05 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 4.28E-04 | 5.35E-05 | | Organic | |
| Organic HAPs | | | | | | | | |
| Acetaldehyde | 2.52E-05 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 1.29E-04 | 1.61E-05 | Vapor | Organic | 75-07-0 |
| Acrolein | 7.88E-06 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 4.04E-05 | 5.05E-06 | Vapor | Organic | 107-02-8 |
| Benzene | 7.76E-04 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 3.98E-03 | 4.97E-04 | Vapor | Organic | 71-43-2 |
| Formaldehyde | 7.89E-05 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 4.04E-04 | 5.05E-05 | Vapor | Organic | 50-00-0 |
| Naphthalene | 1.30E-04 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 6.66E-04 | 8.33E-05 | Particulate | Organic | 91-20-3 |
| Propylene | 2.79E-03 | lb/mmBtu | AP-42 (10/96) Table 3.4-4 | 1.43E-02 | 1.79E-03 | Particulate | Organic | 115-07-1 |
| Toluene | 2.81E-04 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 1.44E-03 | 1.80E-04 | Vapor | Organic | 108-88-3 |
| Xylenes | 1.93E-04 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 9.89E-04 | 1.24E-04 | Vapor | Organic | 1330-20-7 |
| Total Organic HAPs | 4.28E-03 | lb/mmBtu | AP-42 (10/96) Table 3.4-3 | 2.19E-02 | 2.74E-03 | | Organic | |

**SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER**

SWITCHYARD DIESEL ENGINE AUXILIARY GENERATOR EMISSIONS NON-CRITERIA POLLUTANTS

| | |
|------------------------|---------|
| Sulfur Content of Fuel | 0.0015% |
|------------------------|---------|

Description: Emission estimates based on a 750 kW emergency diesel generator using No. 2 fuel oil.
The calculations are based on AP-42 emission factors except as noted.

STACK PARAMETERS:

| | | | |
|------------------------------------|--------|-----------------|-------------------|
| Stack Flue Gas Temperature | 805 | K | |
| Flow Rate | 17,901 | acfm | |
| Flow Rate | 4,786 | scfm | |
| Exit Velocity | 74.62 | ft/sec | |
| Height | 19.98 | ft | |
| Stack diameter (top ID) | 14.00 | inch | |
| Stack area | 1.07 | ft ² | |
| Diesel engine output: | 1013 | hp | |
| Diesel engine output: | 2.58 | mmBtu/hr | 1hp = 2546 Btu/hr |
| Diesel engine input: | 37.4 | gal/hr | 5.1 mmBtu/hr |
| Maximum Annual Hours of Operation: | 250 | hours/year | |

Notes:

No Inorganic HAPs according to AP-42, Section 3.4

Stack heights, temperatures, velocities, and diameters and fuel usage rates obtained from Caterpillar data sheets.

Diesel engine input value in mmBtu/hr is based on the assumption the heating value of diesel fuel is 19,300 Btu/lb with a fuel density of 7.1 lb/gal, using the fuel usage value of 37.4 gal/hr.

A6-75
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
DIESEL SO2 ABSORBER EMERGENCY QUENCH PUMP EMISSIONS NON-CRITERIA POLLUTANTS

| Pollutant | Emission Factor | Units | Source | Hourly Emissions (lb/hr) | Annual Emissions (ton/yr) | Pollutant Form | Pollutant Class | Chemical Abstract Services (CAS) Number |
|---------------------------|-----------------|----------|------------------------------|--------------------------|---------------------------|----------------|-----------------|---|
| PAHs | | | | | | | | |
| Acenaphthene | 1.42E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 5.66E-06 | 7.08E-07 | Particulate | Organic | 83-32-9 |
| Acenaphthylene | 5.06E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.02E-05 | 2.52E-06 | Particulate | Organic | 208-96-8 |
| Anthracene | 1.87E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 7.46E-06 | 9.32E-07 | Particulate | Organic | 120-12-7 |
| Benzo(a)anthracene | 1.68E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 6.70E-06 | 8.37E-07 | Particulate | Organic | 56-55-3 |
| Benzo(a)pyrene | 1.88E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 7.50E-07 | 9.37E-08 | Particulate | Organic | 50-32-8 |
| Benzo(b)fluoranthene | 9.91E-08 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 3.95E-07 | 4.94E-08 | Particulate | Organic | 205-99-2 |
| Benzo(k)fluoranthene | 1.55E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 6.18E-07 | 7.73E-08 | Particulate | Organic | 207-08-9 |
| Benzo(g,h,i)perylene | 4.89E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.95E-06 | 2.44E-07 | Particulate | Organic | 191-24-2 |
| Chrysene | 3.53E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.41E-06 | 1.76E-07 | Particulate | Organic | 218-01-9 |
| Dibenz(a,h)anthracene | 5.83E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.32E-06 | 2.91E-07 | Particulate | Organic | 53-70-3 |
| Fluoranthene | 7.61E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 3.03E-05 | 3.79E-06 | Particulate | Organic | 206-44-0 |
| Fluorene | 2.92E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.16E-04 | 1.46E-05 | Particulate | Organic | 86-73-7 |
| Indeno(1,2,3-cd)pyrene | 3.75E-07 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.50E-06 | 1.87E-07 | Particulate | Organic | 193-39-5 |
| Phenanthrene | 2.94E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.17E-04 | 1.47E-05 | Particulate | Organic | 85-01-8 |
| Pyrene | 4.78E-06 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.91E-05 | 2.38E-06 | Particulate | Organic | 129-00-0 |
| Total PAH | 8.33E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 3.32E-04 | 4.15E-05 | | Organic | |
| Organic HAPs | | | | | | | | |
| Acetaldehyde | 7.67E-04 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 3.06E-03 | 3.82E-04 | Vapor | Organic | 75-07-0 |
| Acrolein | 9.25E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 3.69E-04 | 4.61E-05 | Vapor | Organic | 107-02-8 |
| Benzene | 9.33E-04 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 3.72E-03 | 4.65E-04 | Vapor | Organic | 71-43-2 |
| 1,3-Butadiene | 3.91E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.56E-04 | 1.95E-05 | Vapor | Organic | 106-99-0 |
| Formaldehyde | 1.18E-03 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 4.71E-03 | 5.88E-04 | Vapor | Organic | 50-00-0 |
| Naphthalene | 8.48E-05 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 3.38E-04 | 4.23E-05 | Particulate | Organic | 91-20-3 |
| Propylene | 2.58E-03 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.03E-02 | 1.29E-03 | Particulate | Organic | 115-07-1 |
| Toluene | 4.09E-04 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.63E-03 | 2.04E-04 | Vapor | Organic | 108-88-3 |
| Xylenes | 2.85E-04 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 1.14E-03 | 1.42E-04 | Vapor | Organic | 1330-20-7 |
| Total Organic HAPs | 6.37E-03 | lb/mmBtu | AP-42 (10/96) Table 3.3-2 | 2.54E-02 | 3.18E-03 | | Organic | |

A6-75
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
DIESEL SO2 ABSORBER EMERGENCY QUENCH PUMP EMISSIONS NON-CRITERIA POLLUTANTS

| | |
|------------------------|---------|
| Sulfur Content of Fuel | 0.0015% |
|------------------------|---------|

Description: Emission estimates are for a 682.5 HP diesel driven fire pump.
Calculations are based on AP-42 emission factors.

STACK PARAMETERS:

| | | | | |
|------------------------------------|--------|-----------------|-----------------|----------|
| Stack Flue Gas Temperature | 811 | K | | |
| Flow Rate | 11,675 | acfm | | |
| Flow Rate | 3,100 | scfm | | |
| Exit Velocity | 65.78 | ft/sec | | |
| Height | 10.00 | ft | | |
| Stack diameter (top ID) | 12.00 | inch | | |
| Stack area | 0.79 | ft ² | | |
| Diesel engine output: | 683 | HP | 1hp=2546 Btu/hr | |
| Diesel engine output: | 1.74 | mmBtu/hr | | |
| Diesel engine input: | 29.1 | gal/hr | 4.0 | mmBtu/hr |
| Maximum Annual Hours of Operation: | 250 | hours/year | | |

Notes:
No Inorganic HAPs according to AP-42, Section 3.3
Diesel engine input value in mmBtu/hr is based on the assumption the heating value of diesel fuel is 19,300 lb/hr with a fuel density of 7.1 lb/gal, using the fuel usage value of 29.1 gal/hr.

A6-76
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
COAL HANDLING - TOXIC MATERIAL HANDLING EMISSIONS

| FIN # | Emissions Source Description | PM ₁₀ | | Antimony ¹ 0.49 ppm | | Arsenic ¹ 2.6 ppm | | Beryllium ¹ 0.54 ppm | | Cadmium ¹ 0.21 ppm | | Chromium ¹ 6.1 ppm | | Pollutant Form |
|---------------------------|--|------------------|------------|-----------------------------------|------------|---------------------------------|------------|------------------------------------|------------|----------------------------------|------------|----------------------------------|------------|-------------------|
| | | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | |
| New Coal Handling System: | | | | | | | | | | | | | | |
| MDC-1 | Car Dumper Dust Collector | 6.86 | 30.0 | 3.4E-06 | 1.5E-05 | 1.8E-05 | 7.8E-05 | 3.7E-06 | 1.6E-05 | 1.4E-06 | 6.3E-06 | 4.2E-05 | 1.8E-04 | Particulate |
| MDC-2 | Transfer Tower #1 Dust Collector | 0.90 | 3.9 | 4.4E-07 | 1.9E-06 | 2.3E-06 | 1.0E-05 | 4.9E-07 | 2.1E-06 | 1.9E-07 | 8.3E-07 | 5.5E-06 | 2.4E-05 | Particulate |
| MDC-3 | Transfer Tower #2 Dust Collector | 0.90 | 3.9 | 4.4E-07 | 1.9E-06 | 2.3E-06 | 1.0E-05 | 4.9E-07 | 2.1E-06 | 1.9E-07 | 8.3E-07 | 5.5E-06 | 2.4E-05 | Particulate |
| MDC-4 | Crusher Building Dust Collector | 0.99 | 4.3 | 4.8E-07 | 2.1E-06 | 2.6E-06 | 1.1E-05 | 5.3E-07 | 2.3E-06 | 2.1E-07 | 9.1E-07 | 6.0E-06 | 2.6E-05 | Particulate |
| MDC-5 | Transfer Tower #3 Dust Collector | 0.90 | 3.9 | 4.4E-07 | 1.9E-06 | 2.3E-06 | 1.0E-05 | 4.9E-07 | 2.1E-06 | 1.9E-07 | 8.3E-07 | 5.5E-06 | 2.4E-05 | Particulate |
| CDC-1 | Coal Storage Dome #1 Dust Collector (live storage) | 6.43 | 28.2 | 3.2E-06 | 1.4E-05 | 1.7E-05 | 7.3E-05 | 3.5E-06 | 1.5E-05 | 1.4E-06 | 5.9E-06 | 3.9E-05 | 1.7E-04 | Particulate |
| CDC-2 | Coal Storage Dome #2 Dust Collector (live storage) | 6.43 | 28.2 | 3.2E-06 | 1.4E-05 | 1.7E-05 | 7.3E-05 | 3.5E-06 | 1.5E-05 | 1.4E-06 | 5.9E-06 | 3.9E-05 | 1.7E-04 | Particulate |
| CDC-3 | Coal Reclaim Hopper #1 Dust Collector | 0.47 | 2.1 | 2.3E-07 | 1.0E-06 | 1.2E-06 | 5.4E-06 | 2.5E-07 | 1.1E-06 | 9.9E-08 | 4.3E-07 | 2.9E-06 | 1.3E-05 | Particulate |
| CDC-4 | Coal Reclaim Hopper #2 Dust Collector | 0.47 | 2.1 | 2.3E-07 | 1.0E-06 | 1.2E-06 | 5.4E-06 | 2.5E-07 | 1.1E-06 | 9.9E-08 | 4.3E-07 | 2.9E-06 | 1.3E-05 | Particulate |
| CDC-5 | Coal Tripper Floor Unit #1 Dust Collector A | 0.99 | 4.3 | 4.8E-07 | 2.1E-06 | 2.6E-06 | 1.1E-05 | 5.3E-07 | 2.3E-06 | 2.1E-07 | 9.1E-07 | 6.0E-06 | 2.6E-05 | Particulate |
| CDC-6 | Coal Tripper Floor Unit #1 Dust Collector B | 0.99 | 4.3 | 4.8E-07 | 2.1E-06 | 2.6E-06 | 1.1E-05 | 5.3E-07 | 2.3E-06 | 2.1E-07 | 9.1E-07 | 6.0E-06 | 2.6E-05 | Particulate |
| CH-1 | Coal Unloading Belt Feeder Transfer Point | 0.0000 | 0.0000 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | Particulate |
| CH-2 | Coal Stockout Conveyor | 0.07 | 0.3 | 3.4E-08 | 1.5E-07 | 1.8E-07 | 8.0E-07 | 3.8E-08 | 1.7E-07 | 1.5E-08 | 6.5E-08 | 4.3E-07 | 1.9E-06 | Particulate |
| CH-3 | Active Coal Pile Wind Erosion and Maintenance | 1.94 | 8.5 | 9.5E-07 | 4.2E-06 | 5.1E-06 | 2.2E-05 | 1.0E-06 | 4.6E-06 | 4.1E-07 | 1.8E-06 | 1.2E-05 | 5.2E-05 | Particulate |
| CH-4 | Inactive Portion of Coal Pile Wind Erosion | 0.03 | 0.1 | 1.3E-08 | 5.6E-08 | 6.7E-08 | 3.0E-07 | 1.4E-08 | 6.1E-08 | 5.5E-09 | 2.4E-08 | 1.6E-07 | 6.9E-07 | Particulate |
| Total from Coal Handling | | | | 1.4E-05 | 6.1E-05 | 7.4E-05 | 3.2E-04 | 1.5E-05 | 6.7E-05 | 6.0E-06 | 2.6E-05 | 1.7E-04 | 7.6E-04 | |

A6-76
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
COAL HANDLING - TOXIC MATERIAL HANDLING EMISSIONS

| FIN # | Emissions Source Description | PM ₁₀ | | Cobalt ¹ 1.9 ppm | | Chlorine ¹ 118.3 ppm | | Fluorine 43.7 ppm | | Lead ¹ 3 ppm | | Manganese ¹ 26 ppm | | Pollutant Form |
|---------------------------|--|------------------|------------|--------------------------------|------------|------------------------------------|------------|----------------------|------------|----------------------------|------------|----------------------------------|------------|-------------------|
| | | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | |
| New Coal Handling System: | | | | | | | | | | | | | | |
| MDC-1 | Car Dumper Dust Collector | 6.86 | 30.0 | 1.3E-05 | 5.7E-05 | 8.1E-04 | 3.6E-03 | 3.0E-04 | 1.3E-03 | 2.1E-05 | 9.0E-05 | 1.8E-04 | 7.8E-04 | Particulate |
| MDC-2 | Transfer Tower #1 Dust Collector | 0.90 | 3.9 | 1.7E-06 | 7.5E-06 | 1.1E-04 | 4.7E-04 | 3.9E-05 | 1.7E-04 | 2.7E-06 | 1.2E-05 | 2.3E-05 | 1.0E-04 | Particulate |
| MDC-3 | Transfer Tower #2 Dust Collector | 0.90 | 3.9 | 1.7E-06 | 7.5E-06 | 1.1E-04 | 4.7E-04 | 3.9E-05 | 1.7E-04 | 2.7E-06 | 1.2E-05 | 2.3E-05 | 1.0E-04 | Particulate |
| MDC-4 | Crusher Building Dust Collector | 0.99 | 4.3 | 1.9E-06 | 8.2E-06 | 1.2E-04 | 5.1E-04 | 4.3E-05 | 1.9E-04 | 3.0E-06 | 1.3E-05 | 2.6E-05 | 1.1E-04 | Particulate |
| MDC-5 | Transfer Tower #3 Dust Collector | 0.90 | 3.9 | 1.7E-06 | 7.5E-06 | 1.1E-04 | 4.7E-04 | 3.9E-05 | 1.7E-04 | 2.7E-06 | 1.2E-05 | 2.3E-05 | 1.0E-04 | Particulate |
| CDC-1 | Coal Storage Dome #1 Dust Collector (live storage) | 6.43 | 28.2 | 1.2E-05 | 5.3E-05 | 7.6E-04 | 3.3E-03 | 2.8E-04 | 1.2E-03 | 1.9E-05 | 8.4E-05 | 1.7E-04 | 7.3E-04 | Particulate |
| CDC-2 | Coal Storage Dome #2 Dust Collector (live storage) | 6.43 | 28.2 | 1.2E-05 | 5.3E-05 | 7.6E-04 | 3.3E-03 | 2.8E-04 | 1.2E-03 | 1.9E-05 | 8.4E-05 | 1.7E-04 | 7.3E-04 | Particulate |
| CDC-3 | Coal Reclaim Hopper #1 Dust Collector | 0.47 | 2.1 | 9.0E-07 | 3.9E-06 | 5.6E-05 | 2.4E-04 | 2.1E-05 | 9.0E-05 | 1.4E-06 | 6.2E-06 | 1.2E-05 | 5.4E-05 | Particulate |
| CDC-4 | Coal Reclaim Hopper #2 Dust Collector | 0.47 | 2.1 | 9.0E-07 | 3.9E-06 | 5.6E-05 | 2.4E-04 | 2.1E-05 | 9.0E-05 | 1.4E-06 | 6.2E-06 | 1.2E-05 | 5.4E-05 | Particulate |
| CDC-5 | Coal Tripper Floor Unit #1 Dust Collector A | 0.99 | 4.3 | 1.9E-06 | 8.2E-06 | 1.2E-04 | 5.1E-04 | 4.3E-05 | 1.9E-04 | 3.0E-06 | 1.3E-05 | 2.6E-05 | 1.1E-04 | Particulate |
| CDC-6 | Coal Tripper Floor Unit #1 Dust Collector B | 0.99 | 4.3 | 1.9E-06 | 8.2E-06 | 1.2E-04 | 5.1E-04 | 4.3E-05 | 1.9E-04 | 3.0E-06 | 1.3E-05 | 2.6E-05 | 1.1E-04 | Particulate |
| CH-1 | Coal Unloading Belt Feeder Transfer Point | 0.0000 | 0.0000 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | Particulate |
| CH-2 | Coal Stockout Conveyor | 0.07 | 0.3 | 1.3E-07 | 5.8E-07 | 8.3E-06 | 3.6E-05 | 3.1E-06 | 1.3E-05 | 2.1E-07 | 9.2E-07 | 1.8E-06 | 8.0E-06 | Particulate |
| CH-3 | Active Coal Pile Wind Erosion and Maintenance | 1.94 | 8.5 | 3.7E-06 | 1.6E-05 | 2.3E-04 | 1.0E-03 | 8.5E-05 | 3.7E-04 | 5.8E-06 | 2.6E-05 | 5.1E-05 | 2.2E-04 | Particulate |
| CH-4 | Inactive Portion of Coal Pile Wind Erosion | 0.03 | 0.1 | 4.9E-08 | 2.2E-07 | 3.1E-06 | 1.3E-05 | 1.1E-06 | 5.0E-06 | 7.8E-08 | 3.4E-07 | 6.7E-07 | 3.0E-06 | Particulate |
| Total from Coal Handling | | | | 5.4E-05 | 2.4E-04 | 3.4E-03 | 1.5E-02 | 1.2E-03 | 5.4E-03 | 8.5E-05 | 3.7E-04 | 7.4E-04 | 3.2E-03 | |

A6-76
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
COAL HANDLING - TOXIC MATERIAL HANDLING EMISSIONS

| FIN # | Emissions Source Description | PM ₁₀ | | Mercury ¹ 0.130 ppm | | Nickel ¹ 4.6 ppm | | Selenium ¹ 1.10 ppm | | Uranium 1.30 ppm | | Pollutant Form |
|---------------------------|--|------------------|------------|-----------------------------------|------------|--------------------------------|------------|-----------------------------------|------------|---------------------|------------|----------------|
| | | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | |
| New Coal Handling System: | | | | | | | | | | | | |
| MDC-1 | Car Dumper Dust Collector | 6.86 | 30.0 | 8.9E-07 | 3.9E-06 | 3.2E-05 | 1.4E-04 | 7.5E-06 | 3.3E-05 | 8.9E-06 | 3.9E-05 | Particulate |
| MDC-2 | Transfer Tower #1 Dust Collector | 0.90 | 3.9 | 1.2E-07 | 5.1E-07 | 4.1E-06 | 1.8E-05 | 9.9E-07 | 4.3E-06 | 1.2E-06 | 5.1E-06 | Particulate |
| MDC-3 | Transfer Tower #2 Dust Collector | 0.90 | 3.9 | 1.2E-07 | 5.1E-07 | 4.1E-06 | 1.8E-05 | 9.9E-07 | 4.3E-06 | 1.2E-06 | 5.1E-06 | Particulate |
| MDC-4 | Crusher Building Dust Collector | 0.99 | 4.3 | 1.3E-07 | 5.6E-07 | 4.5E-06 | 2.0E-05 | 1.1E-06 | 4.7E-06 | 1.3E-06 | 5.6E-06 | Particulate |
| MDC-5 | Transfer Tower #3 Dust Collector | 0.90 | 3.9 | 1.2E-07 | 5.1E-07 | 4.1E-06 | 1.8E-05 | 9.9E-07 | 4.3E-06 | 1.2E-06 | 5.1E-06 | Particulate |
| CDC-1 | Coal Storage Dome #1 Dust Collector (live storage) | 6.43 | 28.2 | 8.4E-07 | 3.7E-06 | 3.0E-05 | 1.3E-04 | 7.1E-06 | 3.1E-05 | 8.4E-06 | 3.7E-05 | Particulate |
| CDC-2 | Coal Storage Dome #2 Dust Collector (live storage) | 6.43 | 28.2 | 8.4E-07 | 3.7E-06 | 3.0E-05 | 1.3E-04 | 7.1E-06 | 3.1E-05 | 8.4E-06 | 3.7E-05 | Particulate |
| CDC-3 | Coal Reclaim Hopper #1 Dust Collector | 0.47 | 2.1 | 6.1E-08 | 2.7E-07 | 2.2E-06 | 9.5E-06 | 5.2E-07 | 2.3E-06 | 6.1E-07 | 2.7E-06 | Particulate |
| CDC-4 | Coal Reclaim Hopper #2 Dust Collector | 0.47 | 2.1 | 6.1E-08 | 2.7E-07 | 2.2E-06 | 9.5E-06 | 5.2E-07 | 2.3E-06 | 6.1E-07 | 2.7E-06 | Particulate |
| CDC-5 | Coal Tripper Floor Unit #1 Dust Collector A | 0.99 | 4.3 | 1.3E-07 | 5.6E-07 | 4.5E-06 | 2.0E-05 | 1.1E-06 | 4.7E-06 | 1.3E-06 | 5.6E-06 | Particulate |
| CDC-6 | Coal Tripper Floor Unit #1 Dust Collector B | 0.99 | 4.3 | 1.3E-07 | 5.6E-07 | 4.5E-06 | 2.0E-05 | 1.1E-06 | 4.7E-06 | 1.3E-06 | 5.6E-06 | Particulate |
| CH-1 | Coal Unloading Belt Feeder Transfer Point | 0.0000 | 0.0000 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | Particulate |
| CH-2 | Coal Stockout Conveyor | 0.07 | 0.3 | 9.1E-09 | 4.0E-08 | 3.2E-07 | 1.4E-06 | 7.7E-08 | 3.4E-07 | 9.1E-08 | 4.0E-07 | Particulate |
| CH-3 | Active Coal Pile Wind Erosion and Maintenance | 1.94 | 8.5 | 2.5E-07 | 1.1E-06 | 8.9E-06 | 3.9E-05 | 2.1E-06 | 9.4E-06 | 2.5E-06 | 1.1E-05 | Particulate |
| CH-4 | Inactive Portion of Coal Pile Wind Erosion | 0.03 | 0.1 | 3.4E-09 | 1.5E-08 | 1.2E-07 | 5.2E-07 | 2.9E-08 | 1.3E-07 | 3.4E-08 | 1.5E-07 | Particulate |
| Total from Coal Handling | | | | 3.7E-06 | 1.6E-05 | 1.3E-04 | 5.7E-04 | 3.1E-05 | 1.4E-04 | 3.7E-05 | 1.6E-04 | |

Notes:

1 Hazardous Air Pollutant

2 Data source "Section 313 of the Emergency Planning and Community Right-to-Know Act Toxic Chemical Release Inventory Electric Generating Facilities" EPA 745-B-00-004

A6-77
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
LIMESTONE HANDLING - TOXIC MATERIAL HANDLING EMISSIONS

| FIN # | Emissions Source Description | PM ₁₀ | | Arsenic ¹ 2.5 ppm | | Barium 2000 ppm | | Cadmium ¹ 2 ppm | | Chromium ¹ 500 ppm | | Cobalt ¹ 5 ppm | |
|--------------------------------|--|------------------|------------|---------------------------------|------------|--------------------|------------|-------------------------------|------------|----------------------------------|------------|------------------------------|------------|
| | | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year |
| New Limestone Handling System: | | | | | | | | | | | | | |
| LDC-1 | Limestone Preparation Building Dust Collector | 0.17 | 0.75 | 4.3E-07 | 1.9E-06 | 3.4E-04 | 1.5E-03 | 3.4E-07 | 1.5E-06 | 8.6E-05 | 3.8E-04 | 8.6E-07 | 3.8E-06 |
| LDC-2 | Limestone Silo A Dust Collector | 0.06 | 0.26 | 1.5E-07 | 6.6E-07 | 1.2E-04 | 5.3E-04 | 1.2E-07 | 5.3E-07 | 3.0E-05 | 1.3E-04 | 3.0E-07 | 1.3E-06 |
| LDC-3 | Limestone Silo B Dust Collector | 0.06 | 0.26 | 1.5E-07 | 6.6E-07 | 1.2E-04 | 5.3E-04 | 1.2E-07 | 5.3E-07 | 3.0E-05 | 1.3E-04 | 3.0E-07 | 1.3E-06 |
| LDC-4 | Limestone Reclaim Tunnel Dust Collector | 0.18 | 0.77 | 4.4E-07 | 1.9E-06 | 3.5E-04 | 1.5E-03 | 3.5E-07 | 1.5E-06 | 8.8E-05 | 3.9E-04 | 8.8E-07 | 3.9E-06 |
| LDC-5 | Limestone Unloading Building dust collector | 3.21 | 14.08 | 8.0E-06 | 3.5E-05 | 6.4E-03 | 2.8E-02 | 6.4E-06 | 2.8E-05 | 1.6E-03 | 7.0E-03 | 1.6E-05 | 7.0E-05 |
| LH-1 | Limestone Unloading Conveyor Transfer Point | 0.12 | 0.54 | 3.1E-07 | 1.3E-06 | 2.4E-04 | 1.1E-03 | 2.4E-07 | 1.1E-06 | 6.1E-05 | 2.7E-04 | 6.1E-07 | 2.7E-06 |
| LH-2 | Limestone Silo A/B Loading Conveyor Transfer Point | 0.04 | 0.17 | 9.7E-08 | 4.2E-07 | 7.7E-05 | 3.4E-04 | 7.7E-08 | 3.4E-07 | 1.9E-05 | 8.5E-05 | 1.9E-07 | 8.5E-07 |
| LH-3 | Limestone Silo B Loading Conveyor Transfer Point | 0.04 | 0.17 | 9.7E-08 | 4.2E-07 | 7.7E-05 | 3.4E-04 | 7.7E-08 | 3.4E-07 | 1.9E-05 | 8.5E-05 | 1.9E-07 | 8.5E-07 |
| LH-4 | Limestone Pile Wind Erosion and Maintenance | 1.39 | 6.07 | 3.5E-06 | 1.5E-05 | 2.8E-03 | 1.2E-02 | 2.8E-06 | 1.2E-05 | 6.9E-04 | 3.0E-03 | 6.9E-06 | 3.0E-05 |
| Total from Limestone Handling | | | | 1.3E-05 | 5.8E-05 | 1.1E-02 | 4.6E-02 | 1.1E-05 | 4.6E-05 | 2.6E-03 | 1.2E-02 | 2.6E-05 | 1.2E-04 |

A6-77
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
LIMESTONE HANDLING - TOXIC MATERIAL HANDLING EMISSIONS

| FIN # | Emissions Source Description | PM ₁₀ | | Copper 10 ppm | | Lead ¹ 100 ppm | | Manganese ¹ 1100 ppm | | Mercury ¹ 1 ppm | | Nickel ¹ 20.0 ppm | |
|--------------------------------|---|------------------|------------|------------------|------------|------------------------------|------------|------------------------------------|------------|-------------------------------|------------|---------------------------------|------------|
| | | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year |
| New Limestone Handling System: | | | | | | | | | | | | | |
| LDC-1 | Limestone Preparation Building Dust Collector | 0.17 | 0.75 | 1.7E-06 | 7.5E-06 | 1.7E-05 | 7.5E-05 | 1.9E-04 | 8.3E-04 | 1.7E-07 | 7.5E-07 | 3.4E-06 | 1.5E-05 |
| LDC-2 | Limestone Silo A Dust Collector | 0.06 | 0.26 | 6.0E-07 | 2.6E-06 | 6.0E-06 | 2.6E-05 | 6.6E-05 | 2.9E-04 | 6.0E-08 | 2.6E-07 | 1.2E-06 | 5.3E-06 |
| LDC-3 | Limestone Silo B Dust Collector | 0.06 | 0.26 | 6.0E-07 | 2.6E-06 | 6.0E-06 | 2.6E-05 | 6.6E-05 | 2.9E-04 | 6.0E-08 | 2.6E-07 | 1.2E-06 | 5.3E-06 |
| LDC-4 | Limestone Reclaim Tunnel Dust Collector | 0.18 | 0.77 | 1.8E-06 | 7.7E-06 | 1.8E-05 | 7.7E-05 | 1.9E-04 | 8.5E-04 | 1.8E-07 | 7.7E-07 | 3.5E-06 | 1.5E-05 |
| LDC-5 | Limestone Unloading Building dust collector | 3.21 | 14.08 | 3.2E-05 | 1.4E-04 | 3.2E-04 | 1.4E-03 | 3.5E-03 | 1.5E-02 | 3.2E-06 | 1.4E-05 | 6.4E-05 | 2.8E-04 |
| LH-1 | Limestone Unloading Conveyor Transfer Point | 0.12 | 0.54 | 1.2E-06 | 5.4E-06 | 1.2E-05 | 5.4E-05 | 1.3E-04 | 5.9E-04 | 1.2E-07 | 5.4E-07 | 2.4E-06 | 1.1E-05 |
| LH-2 | Limestone Silo A/B Loading Conveyor Transfer Point | 0.04 | 0.17 | 3.9E-07 | 1.7E-06 | 3.9E-06 | 1.7E-05 | 4.3E-05 | 1.9E-04 | 3.9E-08 | 1.7E-07 | 7.7E-07 | 3.4E-06 |
| LH-3 | Limestone Silo B Loading Conveyor Transfer Point | 0.04 | 0.17 | 3.9E-07 | 1.7E-06 | 3.9E-06 | 1.7E-05 | 4.3E-05 | 1.9E-04 | 3.9E-08 | 1.7E-07 | 7.7E-07 | 3.4E-06 |
| LH-4 | Limestone Pile Wind Erosion and Maintenance | 1.39 | 6.07 | 1.4E-05 | 6.1E-05 | 1.4E-04 | 6.1E-04 | 1.5E-03 | 6.7E-03 | 1.4E-06 | 6.1E-06 | 2.8E-05 | 1.2E-04 |
| Total from Limestone Handling | | | | 5.3E-05 | 2.3E-04 | 5.3E-04 | 2.3E-03 | 5.8E-03 | 2.5E-02 | 5.3E-06 | 2.3E-05 | 1.1E-04 | 4.6E-04 |

A6-77
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
LIMESTONE HANDLING - TOXIC MATERIAL HANDLING EMISSIONS

| FIN # | Limestone ² Emissions Source Description | PM ₁₀ | | Selenium ¹ 0.1 ppm | | Silver 1.0 ppm | | Zinc 200.00 ppm | | Pollutant Form | Pollutant Class |
|--------------------------------|---|------------------|------------|----------------------------------|------------|-------------------|------------|--------------------|------------|-------------------|--------------------|
| | | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | | |
| New Limestone Handling System: | | | | | | | | | | | |
| LDC-1 | Limestone Preparation Building Dust Collector | 0.17 | 0.75 | 1.4E-08 | 6.0E-08 | 1.7E-07 | 7.5E-07 | 3.4E-05 | 1.5E-04 | Particulate | Inorganic |
| LDC-2 | Limestone Silo A Dust Collector | 0.06 | 0.26 | 4.8E-09 | 2.1E-08 | 6.0E-08 | 2.6E-07 | 1.2E-05 | 5.3E-05 | Particulate | Inorganic |
| LDC-3 | Limestone Silo B Dust Collector | 0.06 | 0.26 | 4.8E-09 | 2.1E-08 | 6.0E-08 | 2.6E-07 | 1.2E-05 | 5.3E-05 | Particulate | Inorganic |
| LDC-4 | Limestone Reclaim Tunnel Dust Collector | 0.18 | 0.77 | 1.4E-08 | 6.2E-08 | 1.8E-07 | 7.7E-07 | 3.5E-05 | 1.5E-04 | Particulate | Inorganic |
| LDC-5 | Limestone Unloading Building dust collector | 3.21 | 14.08 | 2.6E-07 | 1.1E-06 | 3.2E-06 | 1.4E-05 | 6.4E-04 | 2.8E-03 | Particulate | Inorganic |
| LH-1 | Limestone Unloading Conveyor Transfer Point | 0.12 | 0.54 | 9.8E-09 | 4.3E-08 | 1.2E-07 | 5.4E-07 | 2.4E-05 | 1.1E-04 | Particulate | Inorganic |
| LH-2 | Limestone Silo A/B Loading Conveyor Transfer Point | 0.04 | 0.17 | 3.1E-09 | 1.4E-08 | 3.9E-08 | 1.7E-07 | 7.7E-06 | 3.4E-05 | Particulate | Inorganic |
| LH-3 | Limestone Silo B Loading Conveyor Transfer Point | 0.04 | 0.17 | 3.1E-09 | 1.4E-08 | 3.9E-08 | 1.7E-07 | 7.7E-06 | 3.4E-05 | Particulate | Inorganic |
| LH-4 | Limestone Pile Wind Erosion and Maintenance | 1.39 | 6.07 | 1.1E-07 | 4.9E-07 | 1.4E-06 | 6.1E-06 | 2.8E-04 | 1.2E-03 | Particulate | Inorganic |
| Total from Limestone Handling | | | | 4.2E-07 | 1.8E-06 | 5.3E-06 | 2.3E-05 | 1.1E-03 | 4.6E-03 | | |

Notes:

1 Hazardous Air Pollutant

2 Data source "Section 313 of the Emergency Planning and Community Right-to-Know Act Toxic Chemical Release Inventory Electric Generating Facilities" EPA 745-B-00-004

A6-78
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
ASH HANDLING - TOXIC MATERIAL HANDLING EMISSIONS

| FIN # | Emissions Source Description | PM ₁₀ | | Antimony ¹ | | Arsenic ¹ | | Barium | | Cadmium ¹ | | Chromium ¹ | |
|-------------------------------|--|-------------------------|------------|-----------------------|------------|----------------------|------------|-----------|------------|----------------------|------------|-----------------------|------------|
| | | Fly Ash ² | | 131 ppm | | 6300 ppm | | 13800 ppm | | 130 ppm | | 900 ppm | |
| | | Bottom Ash ² | | 10 ppm | | 168 ppm | | 9360 ppm | | 10 ppm | | 5820 ppm | |
| | | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year |
| New Fly Ash Handling System | | | | | | | | | | | | | |
| ACD-1 | Fly Ash Silo 1 Dust Collector | 0.09 | 0.38 | 1.1E-05 | 4.9E-05 | 5.4E-04 | 2.4E-03 | 1.2E-03 | 5.2E-03 | 1.1E-05 | 4.9E-05 | 7.7E-05 | 3.4E-04 |
| ACD-2 | Fly Ash Silo 2 Dust Collector | 0.09 | 0.38 | 1.1E-05 | 4.9E-05 | 5.4E-04 | 2.4E-03 | 1.2E-03 | 5.2E-03 | 1.1E-05 | 4.9E-05 | 7.7E-05 | 3.4E-04 |
| New Bed Ash Handling System | | | | | | | | | | | | | |
| ACD-3 | Bottom Ash Silo 1 Dust Collector | 0.09 | 0.38 | 8.6E-07 | 3.8E-06 | 1.4E-05 | 6.3E-05 | 8.0E-04 | 3.5E-03 | 8.6E-07 | 3.8E-06 | 5.0E-04 | 2.2E-03 |
| ACD-4 | Bottom Ash Silo 2 Dust Collector | 0.09 | 0.38 | 8.6E-07 | 3.8E-06 | 1.4E-05 | 6.3E-05 | 8.0E-04 | 3.5E-03 | 8.6E-07 | 3.8E-06 | 5.0E-04 | 2.2E-03 |
| New Landfill Handling System: | | | | | | | | | | | | | |
| LF-1 | Landfill Inactive Pile Wind Erosion - area 1 | 0.0 | 0.0 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 |
| LF-2 | Landfill Inactive Pile Wind Erosion - area 2 | 0.0 | 0.0 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 |
| LF-3 | Landfill Inactive Pile Wind Erosion - 5 yr cell | 0.0 | 0.0 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 |
| LF-4 | Landfill Stockout | 0.003 | 0.015 | 4.5E-07 | 2.0E-06 | 2.2E-05 | 9.5E-05 | 4.8E-05 | 2.1E-04 | 4.5E-07 | 2.0E-06 | 3.1E-06 | 1.4E-05 |
| LF-5 | Landfill Active Pile Wind Erosion and Maintenance | 2.43 | 10.66 | 3.2E-04 | 1.4E-03 | 1.5E-02 | 6.7E-02 | 3.4E-02 | 1.5E-01 | 3.2E-04 | 1.4E-03 | 2.2E-03 | 9.6E-03 |
| Total from Ash Handling | | | | 3.4E-04 | 1.5E-03 | 1.6E-02 | 7.2E-02 | 3.8E-02 | 1.6E-01 | 3.4E-04 | 1.5E-03 | 3.3E-03 | 1.5E-02 |

A6-78
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
ASH HANDLING - TOXIC MATERIAL HANDLING EMISSIONS

| FIN # | Emissions Source Description | PM ₁₀ | | Copper 2200 ppm 932 ppm | | Lead ¹ 2120 ppm 1082 ppm | | Manganese ¹ 3000 ppm 1940 ppm | | Mercury ¹ 12.0 ppm 4.2 ppm | | Nickel ¹ 4300 ppm 2939 ppm | |
|-------------------------------|---|------------------|------------|-------------------------------|------------|---|------------|--|------------|---|------------|---|------------|
| | | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year |
| New Fly Ash Handling System | | | | | | | | | | | | | |
| ACD-1 | Fly Ash Silo 1 Dust Collector | 0.09 | 0.38 | 1.9E-04 | 8.3E-04 | 1.8E-04 | 8.0E-04 | 2.6E-04 | 1.1E-03 | 1.0E-06 | 4.5E-06 | 3.7E-04 | 1.6E-03 |
| ACD-2 | Fly Ash Silo 2 Dust Collector | 0.09 | 0.38 | 1.9E-04 | 8.3E-04 | 1.8E-04 | 8.0E-04 | 2.6E-04 | 1.1E-03 | 1.0E-06 | 4.5E-06 | 3.7E-04 | 1.6E-03 |
| New Bed Ash Handling System | | | | | | | | | | | | | |
| ACD-3 | Bottom Ash Silo 1 Dust Collector | 0.09 | 0.38 | 8.0E-05 | 3.5E-04 | 9.3E-05 | 4.1E-04 | 1.7E-04 | 7.3E-04 | 3.6E-07 | 1.6E-06 | 2.5E-04 | 1.1E-03 |
| ACD-4 | Bottom Ash Silo 2 Dust Collector | 0.09 | 0.38 | 8.0E-05 | 3.5E-04 | 9.3E-05 | 4.1E-04 | 1.7E-04 | 7.3E-04 | 3.6E-07 | 1.6E-06 | 2.5E-04 | 1.1E-03 |
| New Landfill Handling System: | | | | | | | | | | | | | |
| LF-1 | Landfill Inactive Pile Wind Erosion - area 1 | 0.00 | 0.00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 |
| LF-2 | Landfill Inactive Pile Wind Erosion - area 2 | 0.00 | 0.00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 |
| LF-3 | Landfill Inactive Pile Wind Erosion - 5 yr cell | 0.00 | 0.00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 |
| LF-4 | Landfill Stockout | 0.00 | 0.02 | 7.6E-06 | 3.3E-05 | 7.3E-06 | 3.2E-05 | 1.0E-05 | 4.5E-05 | 4.1E-08 | 1.8E-07 | 1.5E-05 | 6.5E-05 |
| LF-5 | Landfill Active Pile Wind Erosion and Maintenance | 2.43 | 10.66 | 5.4E-03 | 2.3E-02 | 5.2E-03 | 2.3E-02 | 7.3E-03 | 3.2E-02 | 2.9E-05 | 1.3E-04 | 1.0E-02 | 4.6E-02 |
| Total from Ash Handling | | | | 5.9E-03 | 2.6E-02 | 5.7E-03 | 2.5E-02 | 8.2E-03 | 3.6E-02 | 3.2E-05 | 1.4E-04 | 1.2E-02 | 5.1E-02 |

A6-78
SIERRA PACIFIC POWER COMPANY
ELY ENERGY CENTER
ASH HANDLING - TOXIC MATERIAL HANDLING EMISSIONS

| FIN # | Emissions Source Description | PM ₁₀ | | Selenium ¹ | | Silver | | Vanadium | | Zinc | | Pollutant Form | Pollutant Class |
|-------------------------------|--|------------------|------------|-----------------------|------------|-------------------|------------|-----------------------|------------|----------------------|------------|----------------|-----------------------|
| | | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | lb/ hour | tons/ year | | |
| | Fly Ash ² Bottom Ash ² | | | | | | | | | | | | |
| | | | | 134 ppm 14 ppm | | 36 ppm 9.9 ppm | | 1180 ppm 537.0 ppm | | 3500 ppm 1796 ppm | | | |
| New Fly Ash Handling System | | | | | | | | | | | | | |
| ACD-1 | Fly Ash Silo 1 Dust Collector | 0.09 | 0.38 | 1.1E-05 | 5.0E-05 | 3.1E-06 | 1.4E-05 | 1.0E-04 | 4.4E-04 | 3.0E-04 | 1.3E-03 | Particulate | Inorganic |
| ACD-2 | Fly Ash Silo 2 Dust Collector | 0.09 | 0.38 | 1.1E-05 | 5.0E-05 | 3.1E-06 | 1.4E-05 | 1.0E-04 | 4.4E-04 | 3.0E-04 | 1.3E-03 | Particulate | Inorganic |
| New Bed Ash Handling System | | | | | | | | | | | | | |
| ACD-3 | Bottom Ash Silo 1 Dust Collector | 0.09 | 0.38 | 1.2E-06 | 5.3E-06 | 8.5E-07 | 3.7E-06 | 4.6E-05 | 2.0E-04 | 1.5E-04 | 6.7E-04 | Particulate | Inorganic/ Organic |
| ACD-4 | Bottom Ash Silo 2 Dust Collector | 0.09 | 0.38 | 1.2E-06 | 5.3E-06 | 8.5E-07 | 3.7E-06 | 4.6E-05 | 2.0E-04 | 1.5E-04 | 6.7E-04 | Particulate | Inorganic/ Organic |
| New Landfill Handling System: | | | | | | | | | | | | | |
| LF-1 | Landfill Inactive Pile Wind Erosion - area 1 | 0.00 | 0.00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | Particulate | Inorganic |
| LF-2 | Landfill Inactive Pile Wind Erosion - area 2 | 0.00 | 0.00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | Particulate | Inorganic |
| LF-3 | Landfill Inactive Pile Wind Erosion - 5 yr cell | 0.00 | 0.00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | 0.0E+00 | Particulate | Inorganic |
| LF-4 | Landfill Stockout | 0.00 | 0.02 | 4.6E-07 | 2.0E-06 | 1.2E-07 | 5.4E-07 | 4.1E-06 | 1.8E-05 | 1.2E-05 | 5.3E-05 | Particulate | Inorganic |
| LF-5 | Landfill Active Pile Wind Erosion and Maintenance | 2.43 | 10.66 | 3.3E-04 | 1.4E-03 | 8.8E-05 | 3.8E-04 | 2.9E-03 | 1.3E-02 | 8.5E-03 | 3.7E-02 | Particulate | Inorganic |
| Total from Ash Handling | | | | 3.5E-04 | 1.5E-03 | 9.6E-05 | 4.2E-04 | 3.2E-03 | 1.4E-02 | 9.4E-03 | 4.1E-02 | | |

Notes:

1 Hazardous Air Pollutant

2 Data source "Section 313 of the Emergency Planning and Community Right-to-Know Act Toxic Chemical Release Inventory Electric Generating Facilities" EPA 745-B-00-004